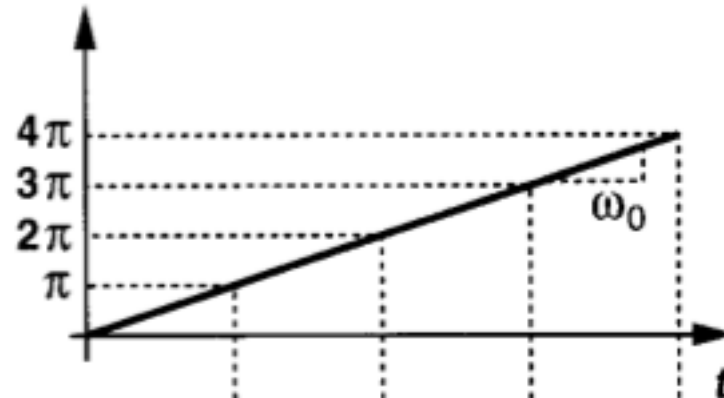

EE4280 Lecture 6: Phase-Locked Loops

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Mathematical Model of VCO

$$\phi(t) = \omega_0 t$$



$$V_0(t) = V_m \sin \omega_0 t$$

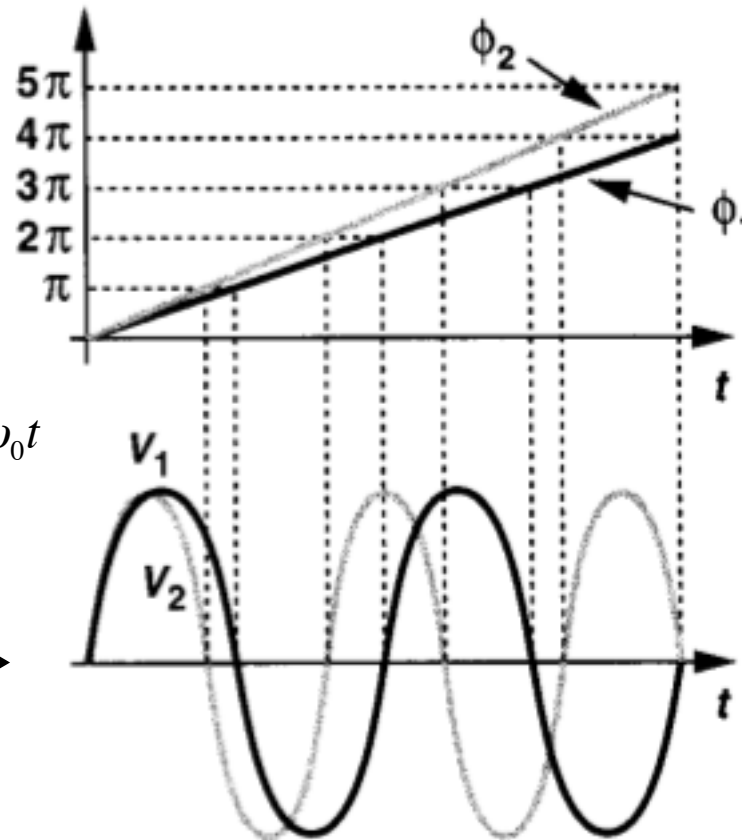
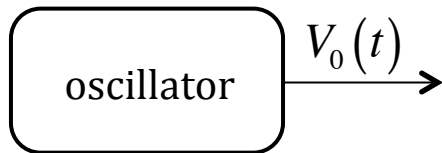


- ◆ Oscillator's output phase is accumulated over time

Mathematical Model of VCO

total phase $\phi(t) = \omega_0 t$

$V_0(t) = V_m \sin \omega_0 t$

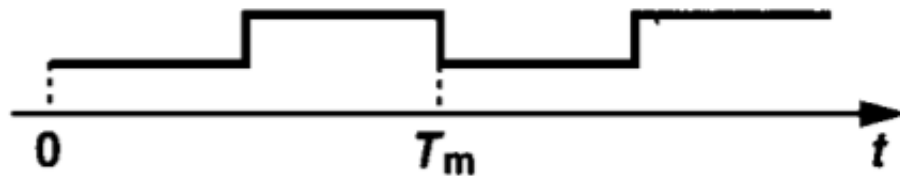


- ◆ Oscillator's output phase is accumulated over time
- ◆ Faster frequency results in faster phase accumulation

From V_{ctrl} to Output Frequency and Phase

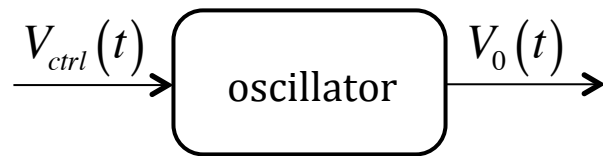
- ◆ Usually a change in V_{ctrl} immediately results in a change in ω_{out}

→ Memoryless



- ◆ If the frequency is a known function of time

Excessive Phase and Transfer Function

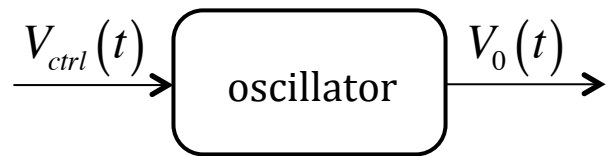


- ◆ Often times, the excessive phase is of interest $\phi_{ex}(t) = K_{VCO} \int V_{ctrl}(t) dt$

➔ Transfer function:

Frequency Modulated Signal

- ◆ With a small sinusoidal control voltage

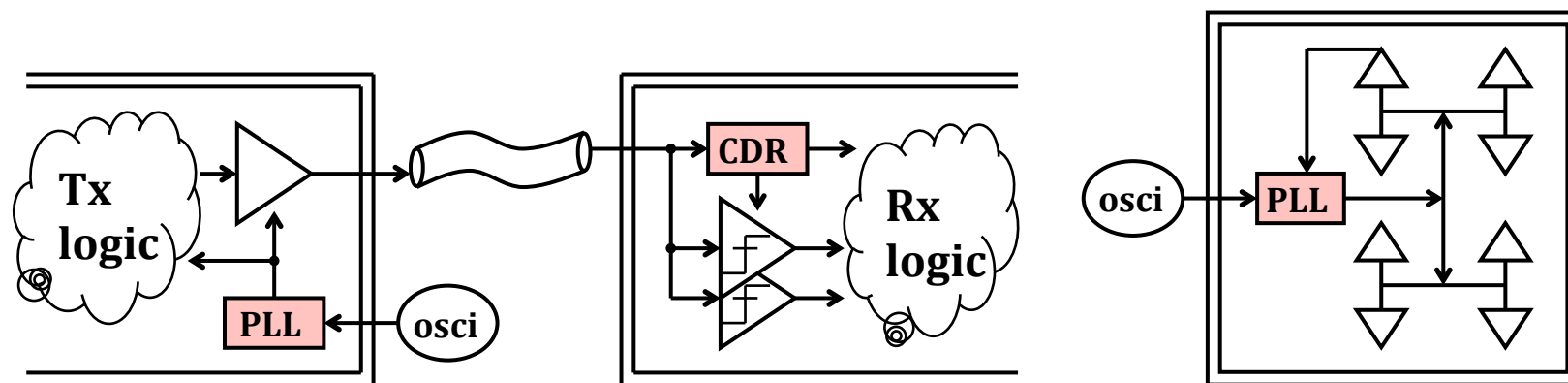


$$V_{cont} = V_m \cos \omega_m t \rightarrow V_{out}(t) = V_0 \cos(\omega_0 t + K_{VCO} \int V_{cont} dt)$$

- ◆ Variation of V_{ctrl} causes unwanted components at output

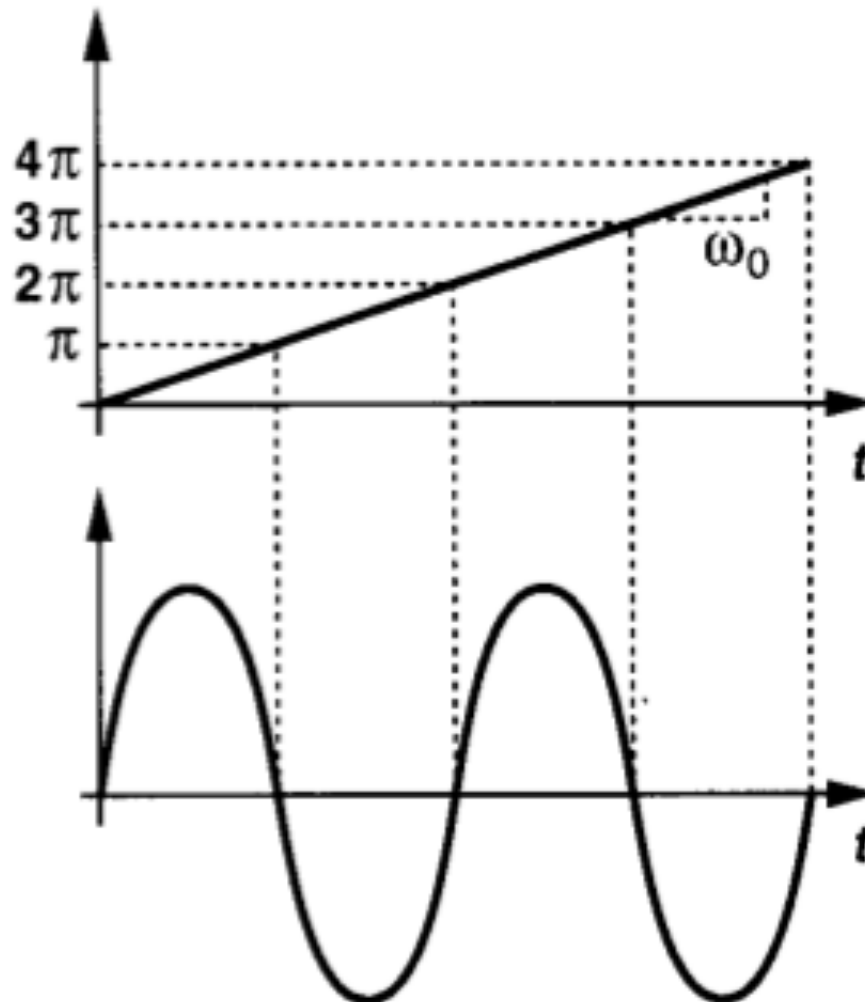
Phase-Locked Loops (I)

- ◆ **Phase-locked loops are used to generate a well-defined clock from a reference source**
- ◆ **Wide range of applications**
 - Clock generation and frequency synthesis
 - Generating a 10GHz clock from a 100MHz reference clock
 - Modulation/demodulation in wireless systems
 - Clock-and-data recovery
 - Extract clock frequency and optimum phase from incoming data stream
 - Skew cancellation
 - Phase aligning an internal clock to an I/O clock

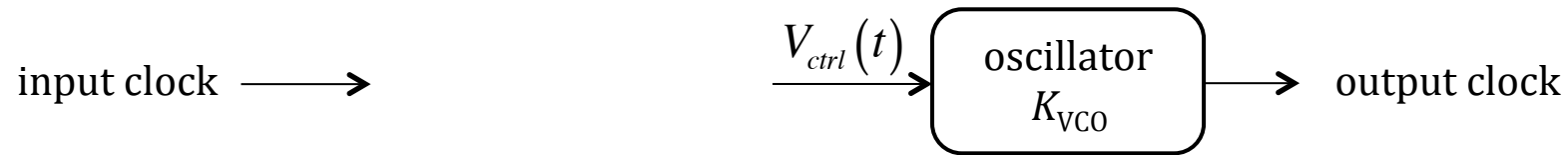


Phase-Locked Loops (II)

- ◆ A **negative feedback system** that compares and adjusts the output phase with the input phase

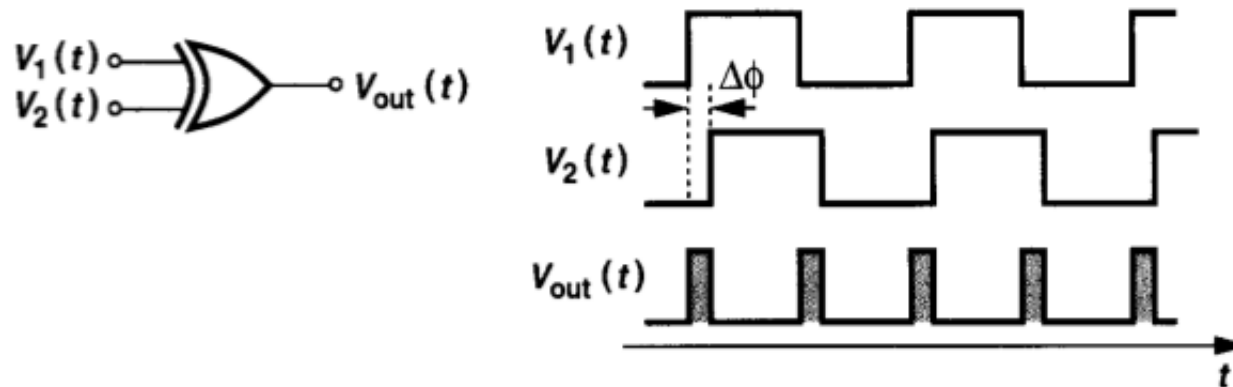


In Order to Achieve Phase Lock



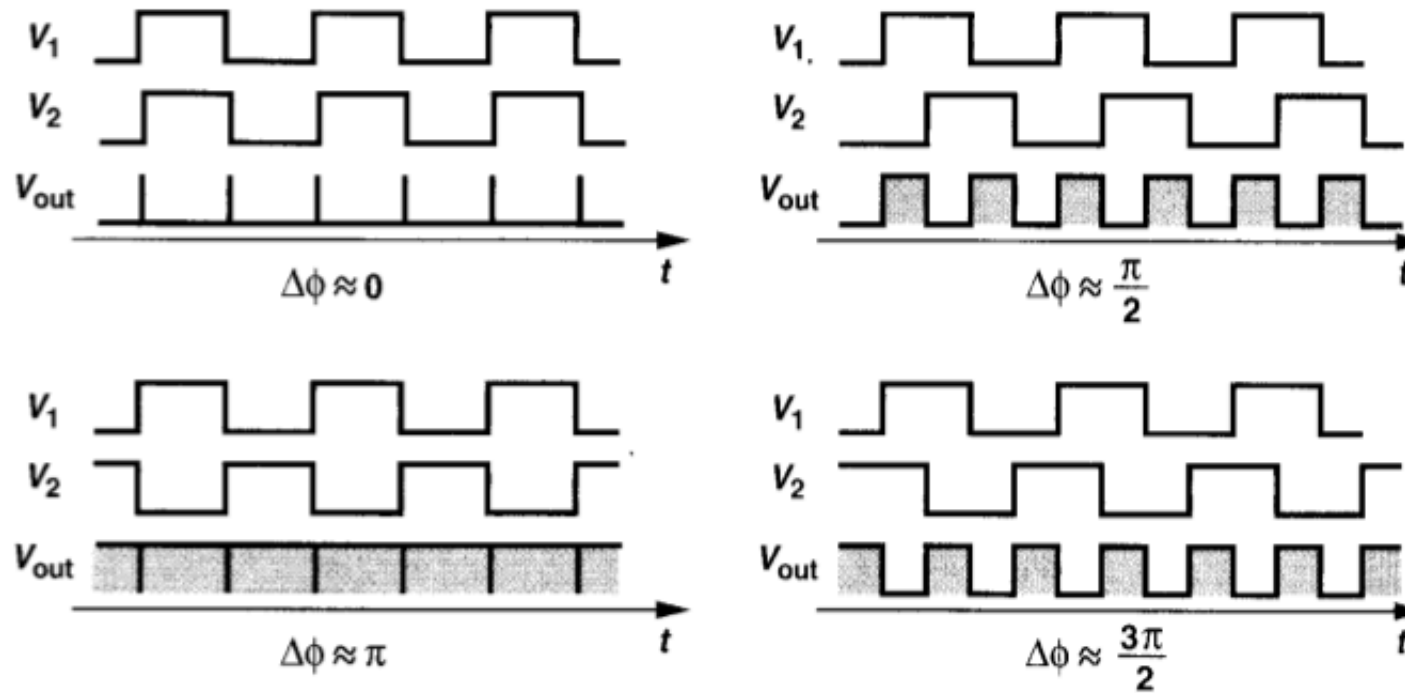
- ◆ Need to measure the phase difference between the two clocks
- ➔ **Phase detector**
A circuit whose average output is linearly proportional to the phase difference between the two inputs
- ➔ We must vary the **frequency** to adjust the phase through integration

Phase Detector Example - XOR Gate (I)



- ◆ Respond to both (rising and falling) edges
- ◆ As the phase difference keeps increasing ...

Phase Detector Example - XOR Gate (II)



- ◆ The phase detector gain K_{PD} of

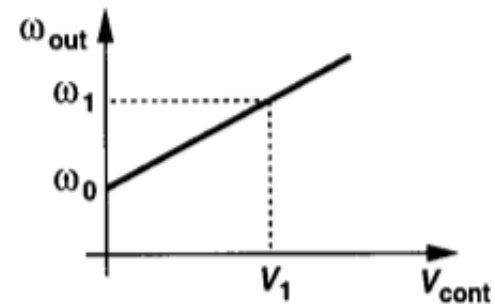
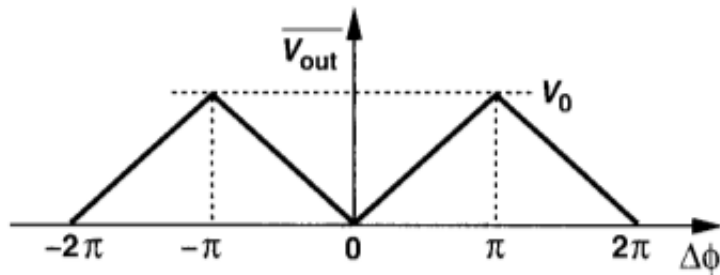
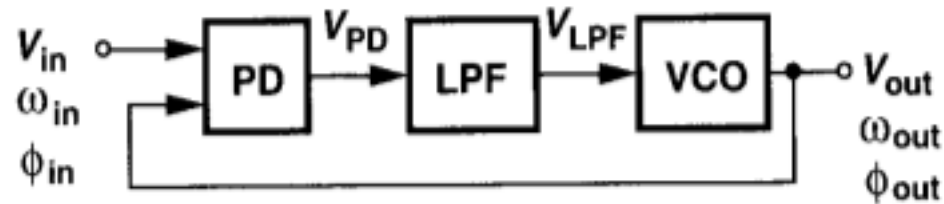
Basic PLL Topology

- ◆ A low-pass filter is used after the phase detector to extract the average PD output

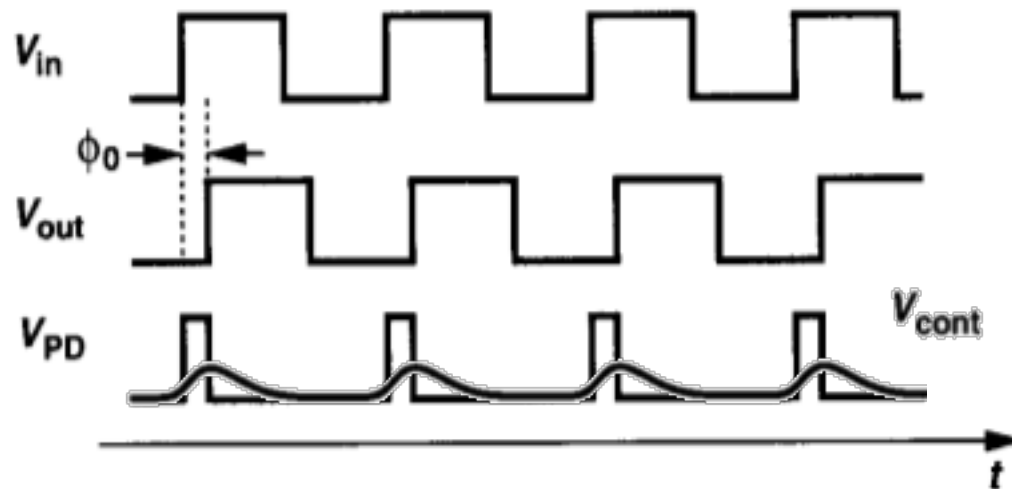
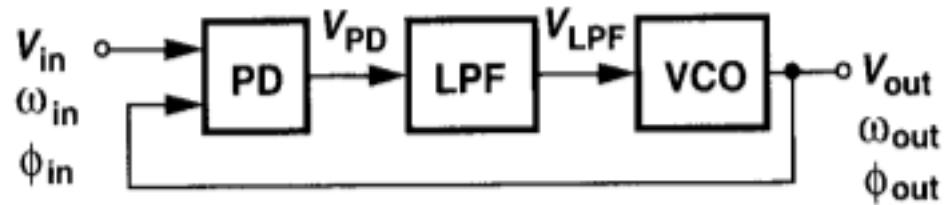
- ◆ In steady state
 - ➔ The **phase** difference settles to small value
 - ➔ The two **frequency** becomes the same

Phase-Locked Loops in Steady State (I)

- ◆ Transfer functions of each building block



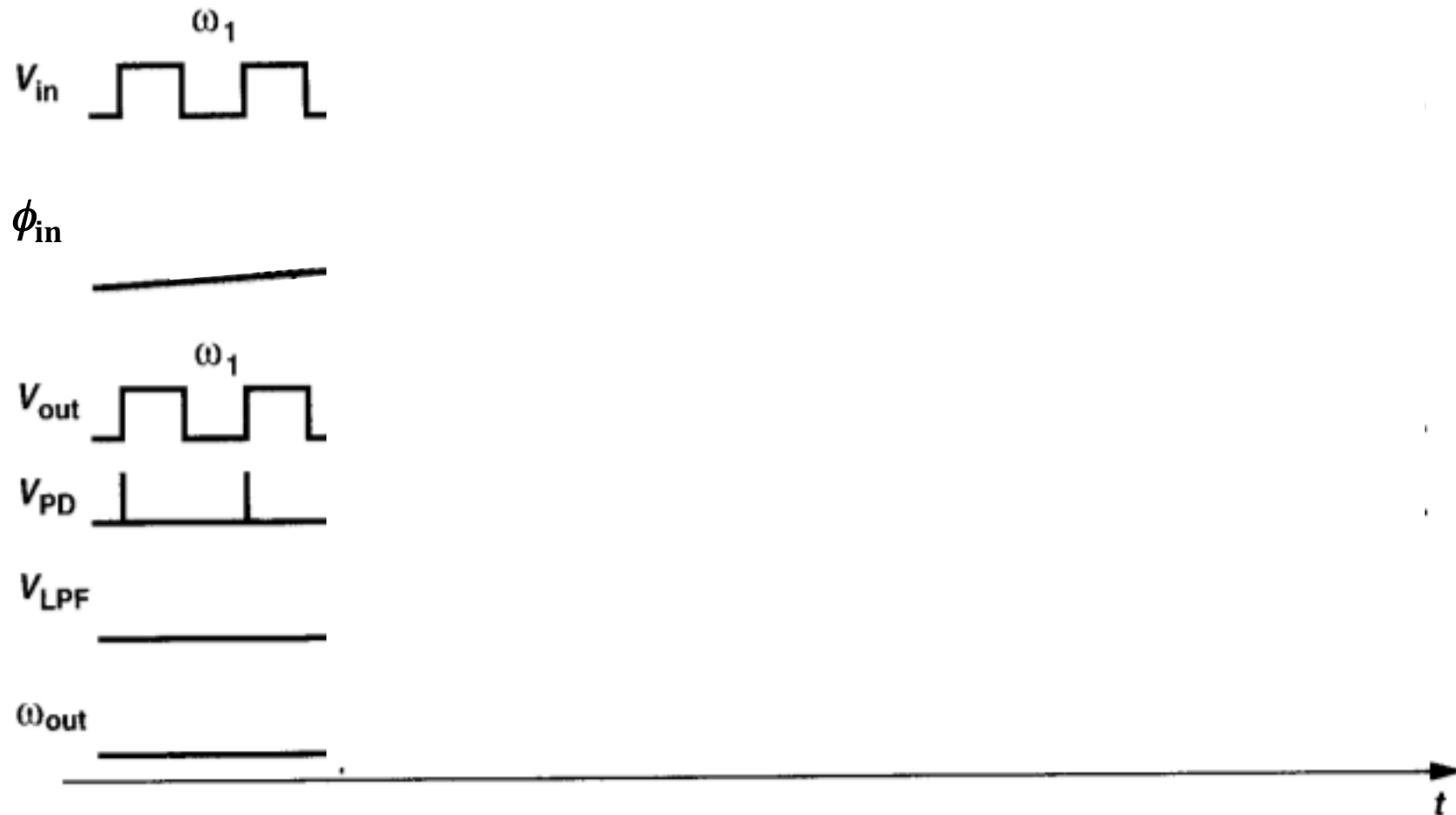
Phase-Locked Loops in Steady State (II)



- ◆ The resulting phase error depends on the operating frequency
- ◆ To minimize phase error $\rightarrow K_{PD}K_{VCO}$ needs to be maximized
- ◆ About operating frequency...

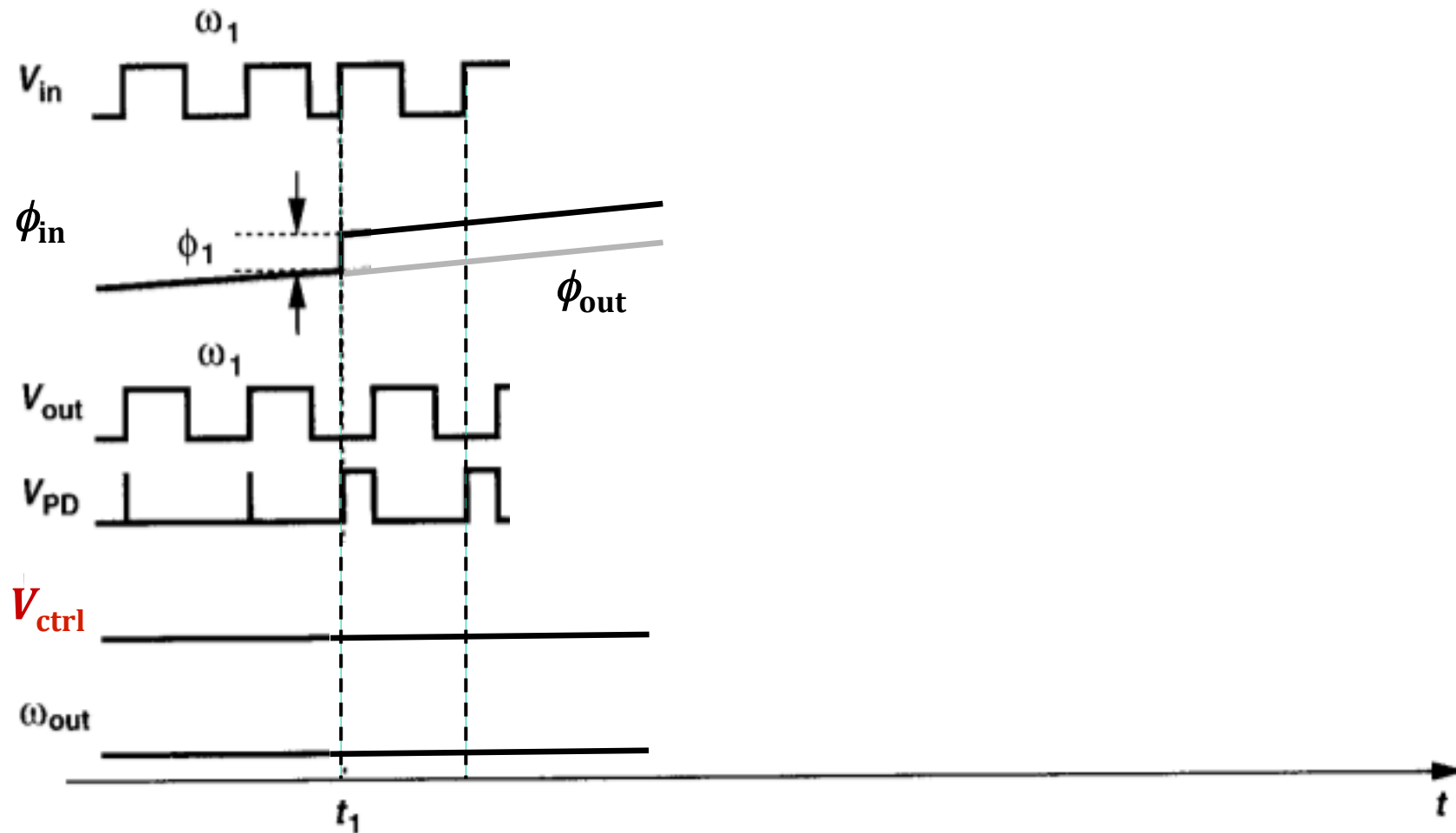
In Case with a Phase Jump

- ◆ How does it look like for a **phase** jump?



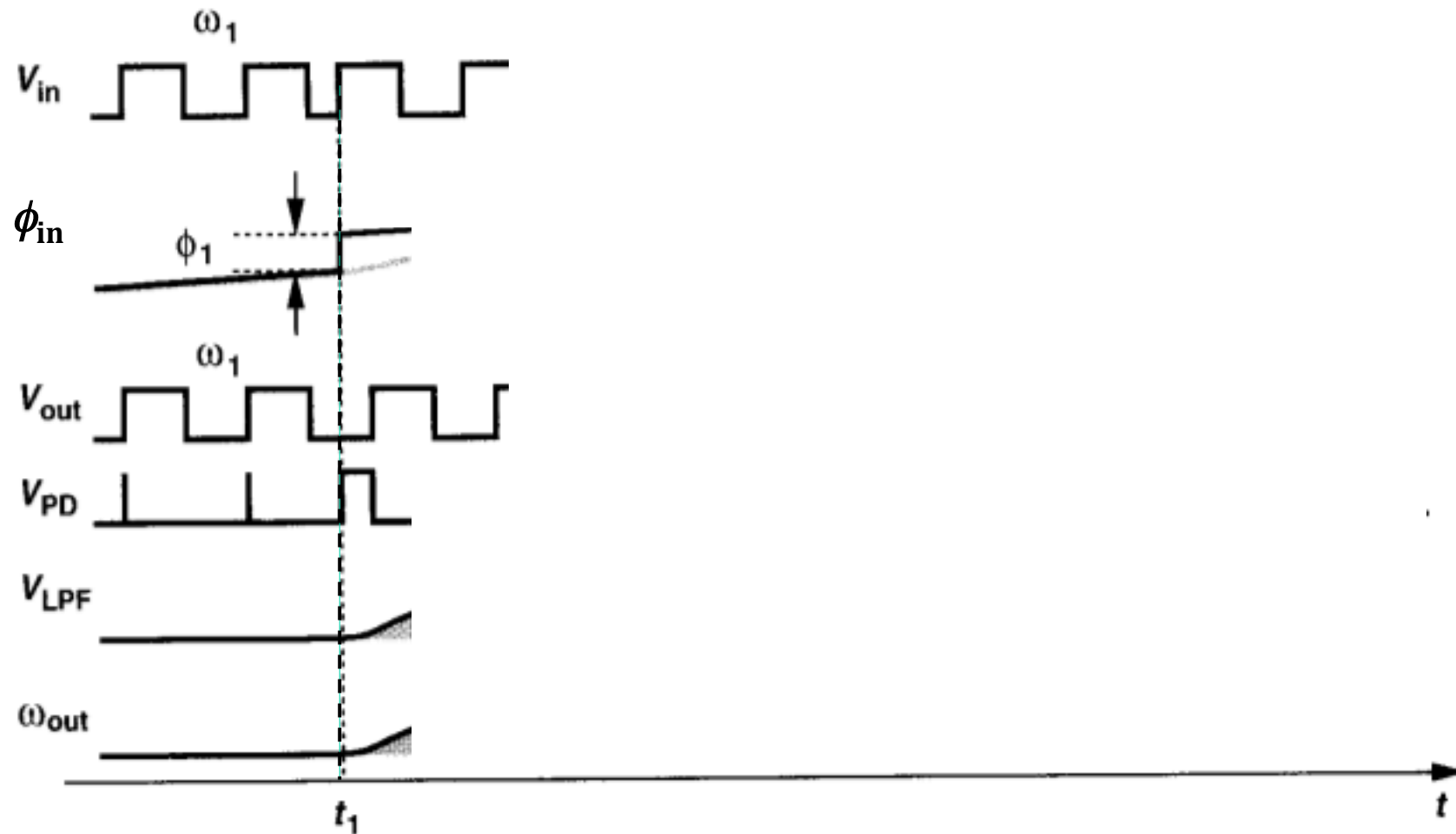
In Case with a Phase Jump

- ◆ How does it look like for a phase jump?
- ◆ @ t_1 if open-loop



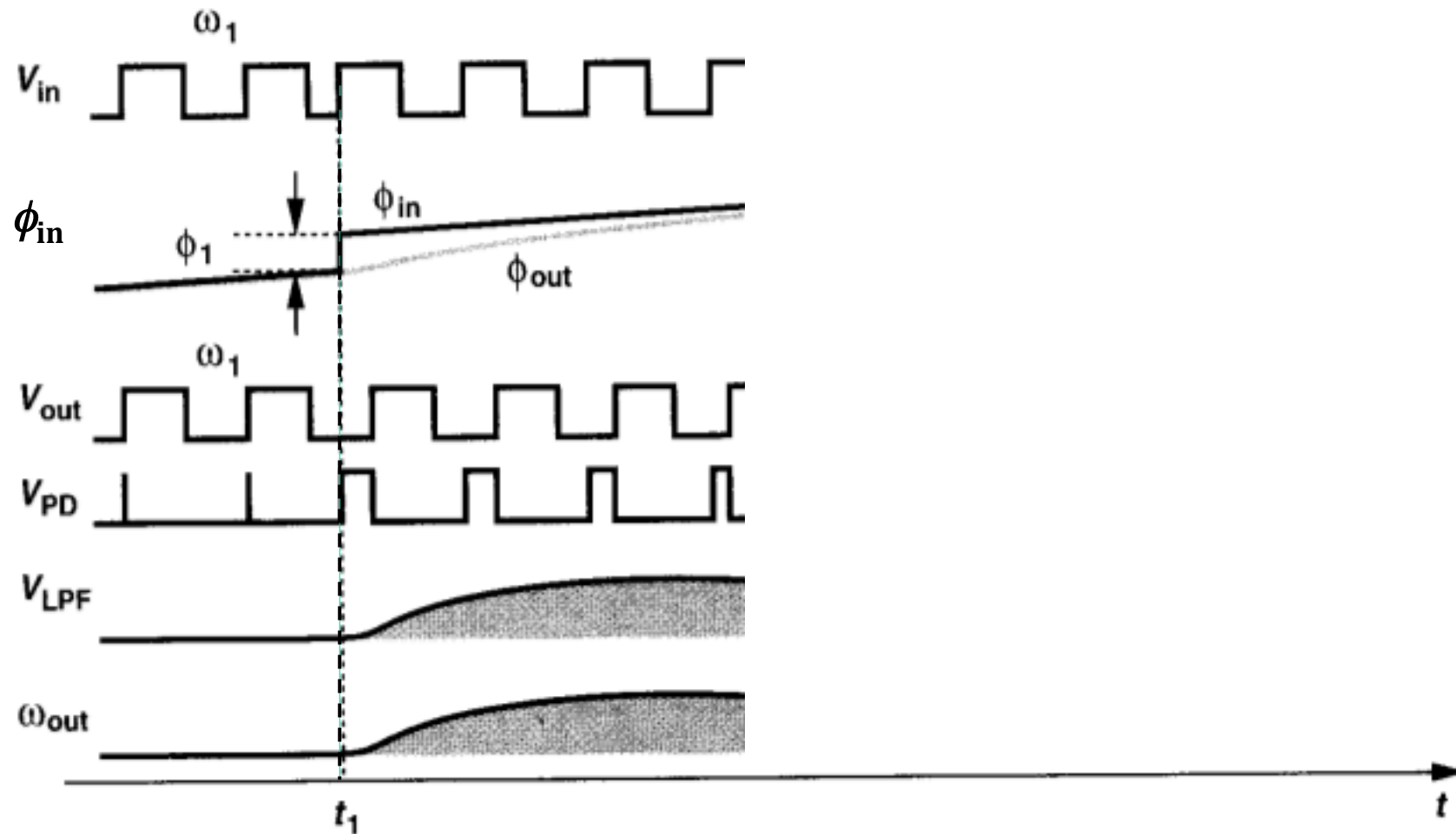
In Case with a Phase Jump

- ◆ How does it look like for a phase jump?
- ◆ @ t_1 with feedback loop



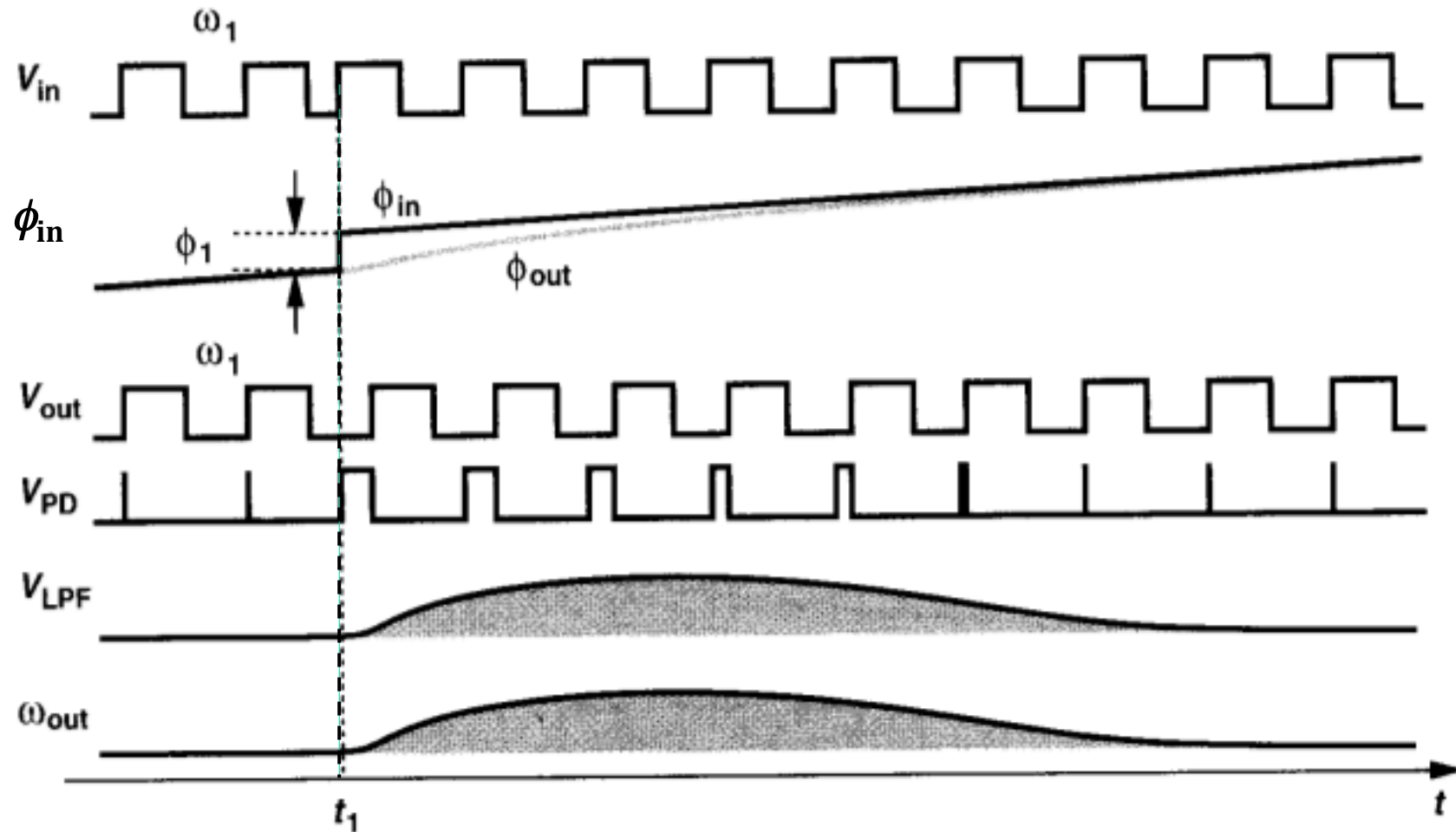
In Case with a Phase Jump

- ◆ How does it look like for a phase jump?
- ◆ **With feedback loop**



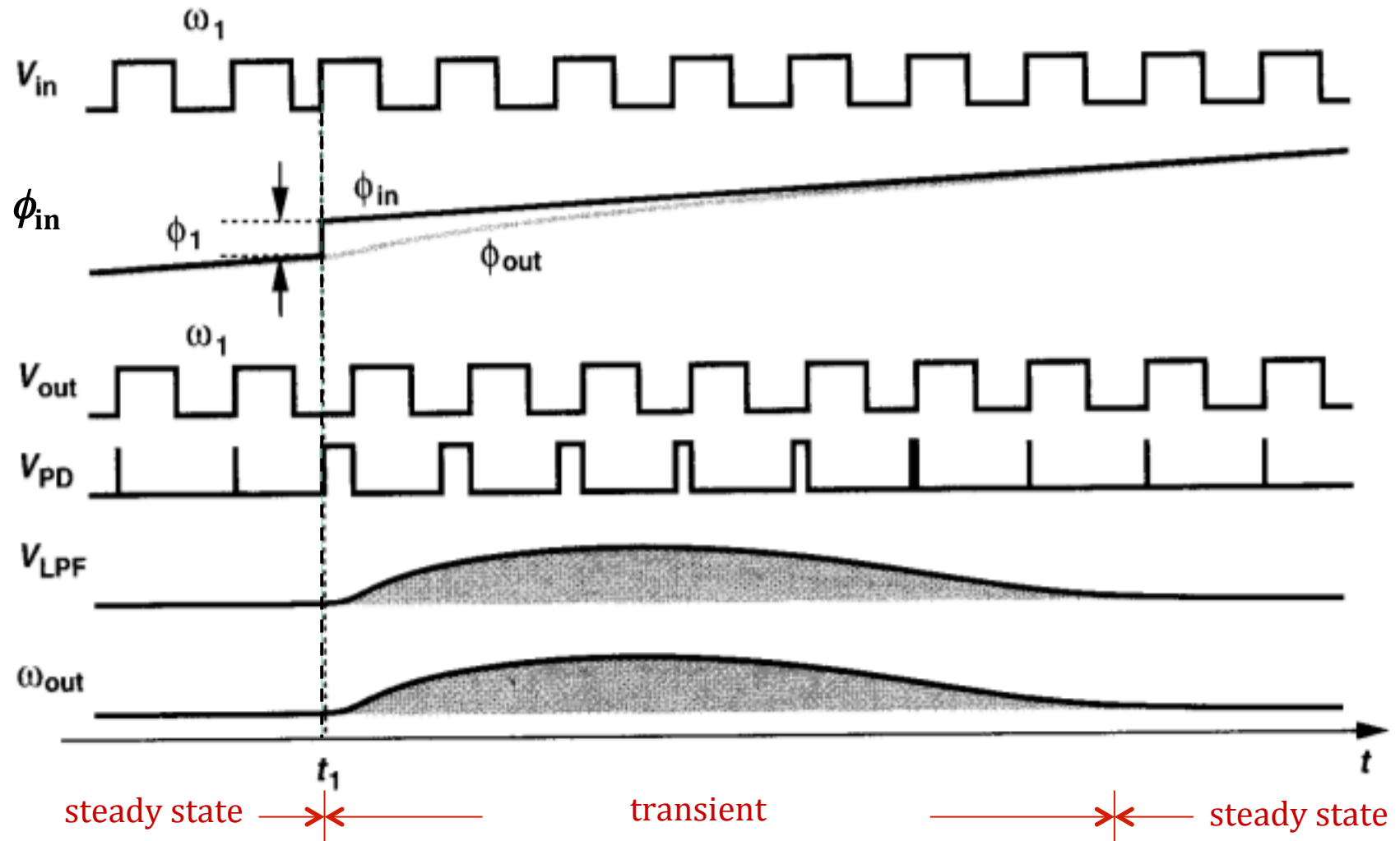
In Case with a Phase Jump

- ◆ How does it look like for a phase jump?
- ◆ **With feedback loop**

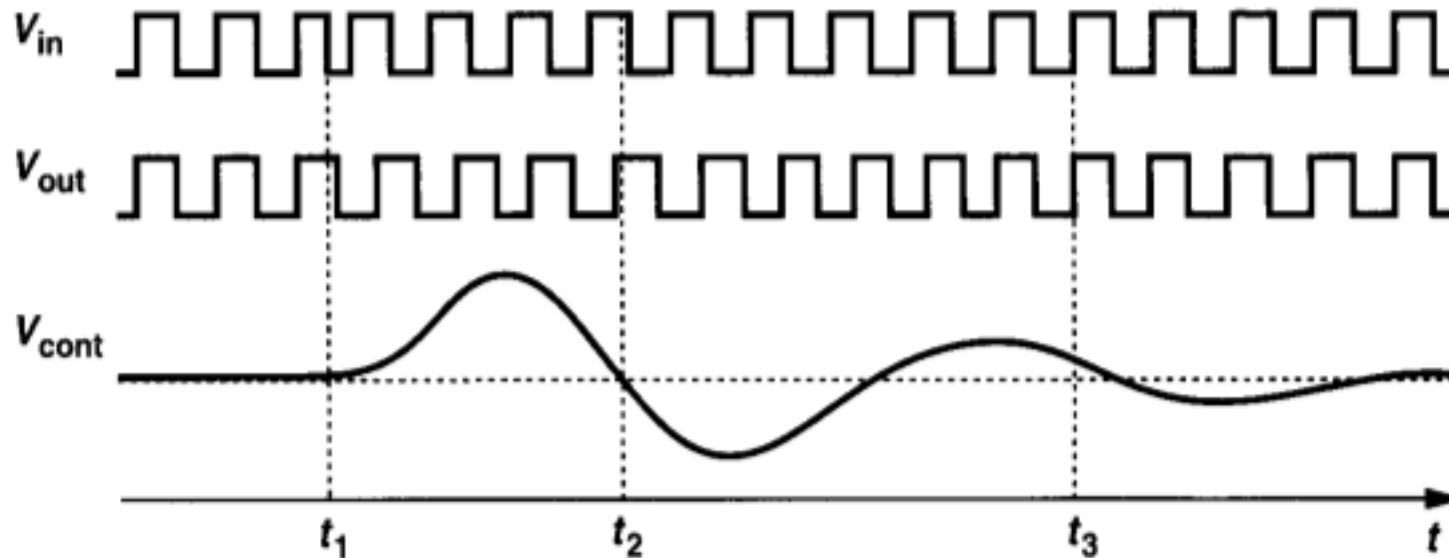


In Case with a Phase Jump

- ◆ How does it look like for a phase jump?
- ◆ **With feedback loop**



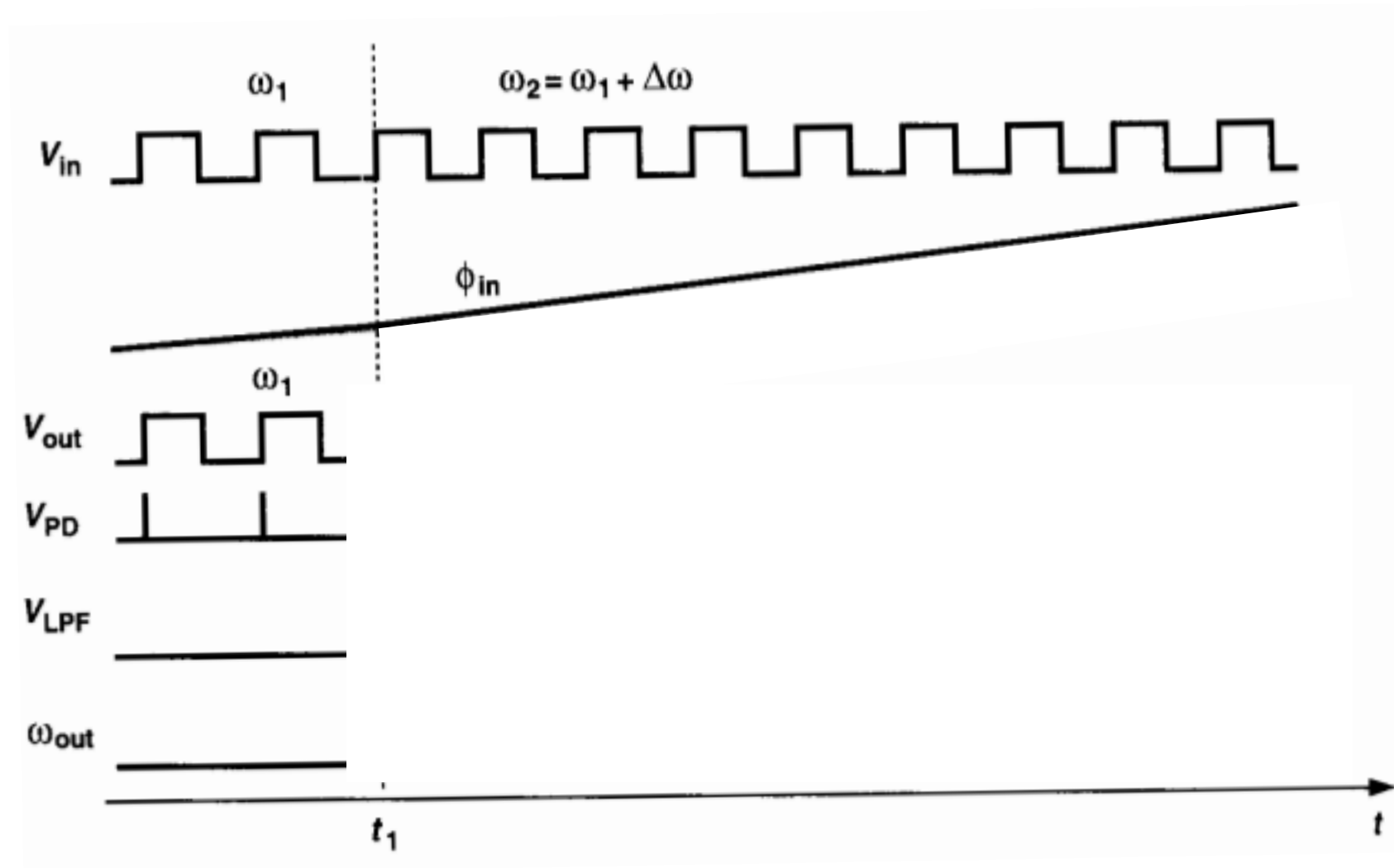
Underdamped Response to Phase Step



- ◆ @ t_1 the phase jump happens
- ◆ @ t_2 the frequencies are the same, but large phase error
- ◆ @ t_3 the phase is the same, but frequency is not

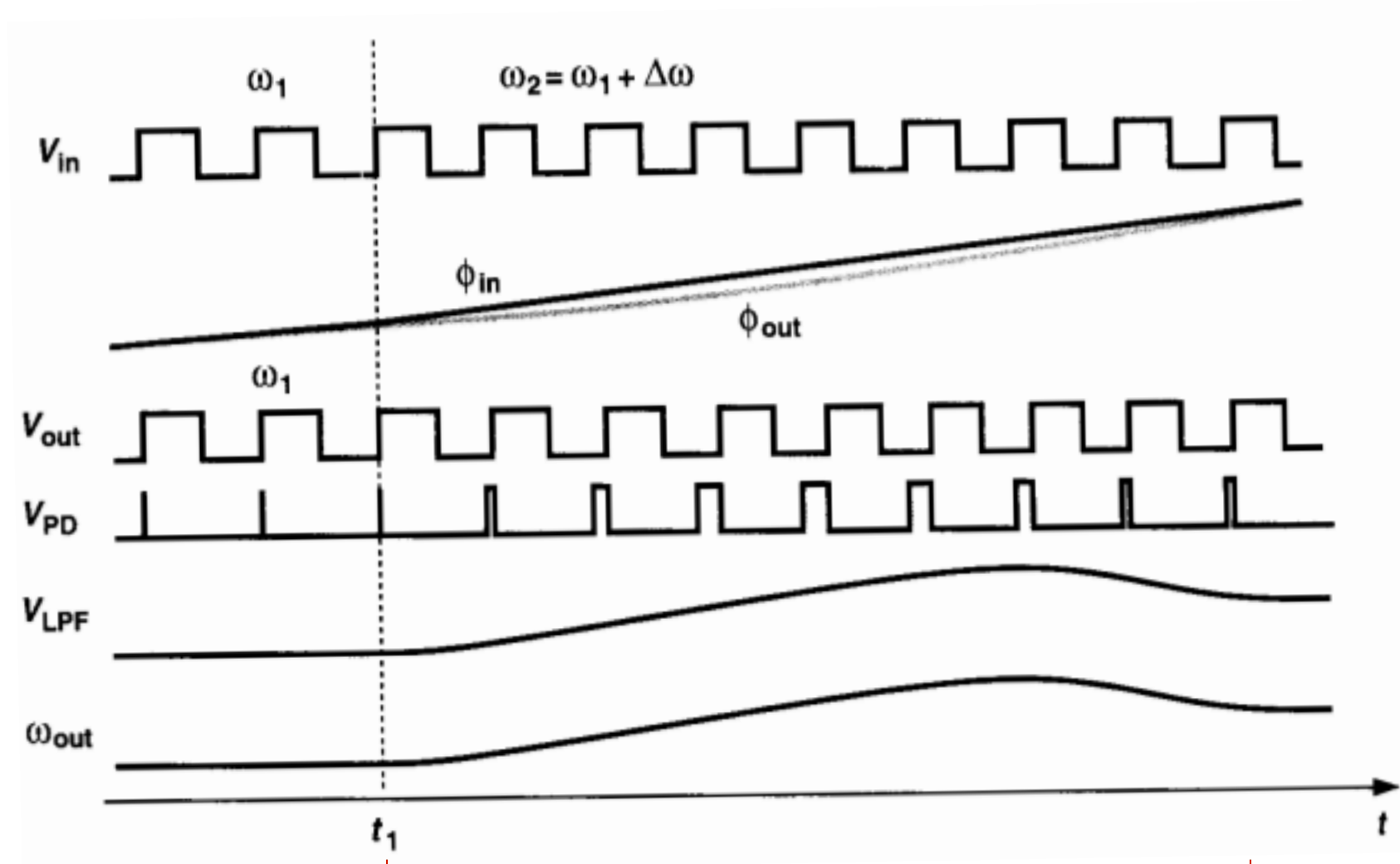
In Case with a Frequency Jump

- ◆ How does it look like for a **frequency** jump?



In Case with a Frequency Jump

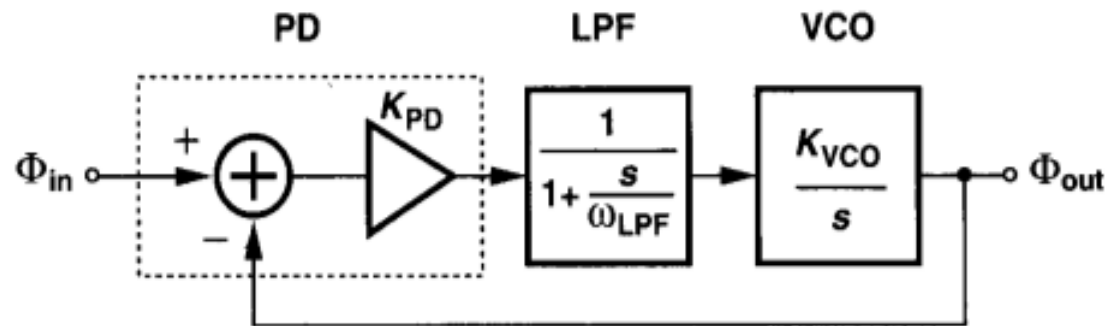
- ◆ How does it look like for a **frequency** jump?



steady state \longleftrightarrow t_1 \longleftrightarrow transient \longleftrightarrow steady state

Loop Dynamics (I)

- ◆ From previous examples, how fast the loop responses depends on the design of the low-pass filter
- ◆ Linear model of the PLL → to derive the response from $\phi_{ex,in}$ to $\phi_{ex,out}$



- ◆ **Open-loop transfer function** (from phase → voltage → voltage → phase)

$$H(s)|_{open} = K_{PD} \cdot \frac{1}{1 + \frac{s}{\omega_{LPF}}} \cdot \frac{K_{VCO}}{s}$$

- Low-frequency gain approaches infinity

Loop Dynamics (II)

◆ Closed-loop transfer function

$$H(s)|_{\text{closed}} = \frac{K_{PD}K_{VCO}}{\frac{s^2}{\omega_{LPF}} + s + K_{PD}K_{VCO}}$$

- Low-frequency gain of unity
- Output tracks the input **phase** well if input phase varies slowly
- For input phase step, output phase eventually catches up

◆ In fact

$$\frac{\omega_{out}}{\omega_{in}}(s) = \frac{K_{PD}K_{VCO}}{\frac{s^2}{\omega_{LPF}} + s + K_{PD}K_{VCO}}$$

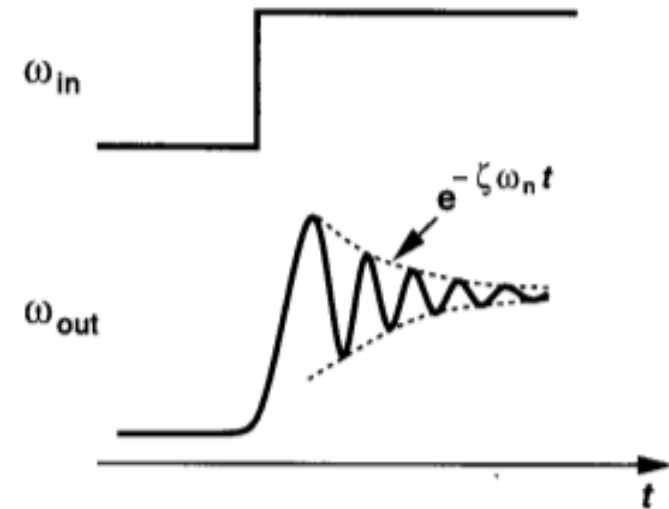
- Low-frequency gain of unity
- Output tracks the input **frequency** well if input frequency varies slowly
- For input frequency step, output frequency eventually catches up

Loop Dynamics (III)

◆ Second-order transfer function

$$H(s)|_{\text{closed}} = \frac{K_{PD}K_{VCO}}{\frac{s^2}{\omega_{LPF}} + s + K_{PD}K_{VCO}} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

$$\omega_n = \sqrt{\omega_{LPF}K_{PD}K_{VCO}} \quad \zeta = \frac{1}{2} \sqrt{\frac{\omega_{LPF}}{K_{PD}K_{VCO}}}$$



- If $\zeta > 1$, both poles are real \rightarrow the system is over damped
- If $\zeta < 1$, both poles are complex \rightarrow the step response can be written as

$$s_{1,2} = -\zeta\omega_n \pm \sqrt{(\zeta^2 - 1)\omega_n^2}$$

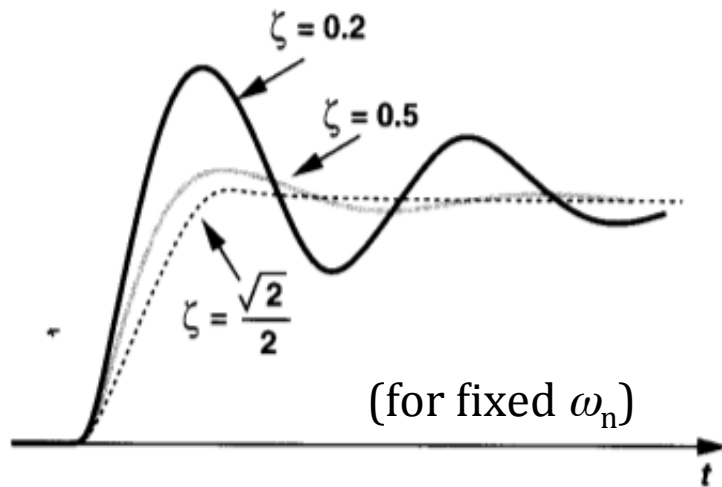
$$\omega_{out}(t) = \left[1 - \frac{1}{\sqrt{1 - \zeta^2}} e^{-\zeta\omega_n t} \sin(\omega_n \sqrt{1 - \zeta^2} t + \theta)\right] \Delta\omega_{ou}(t)$$

(the same behavior for response to phase step)

- Settling speed $\rightarrow \zeta\omega_n$ needs to be maximized

Loop Dynamics (IV)

- ◆ Damping factor ζ



$$\omega_n = \sqrt{\omega_{LPF} K_{PD} K_{VCO}}$$

$$\zeta = \frac{1}{2} \sqrt{\frac{\omega_{LPF}}{K_{PD} K_{VCO}}}$$

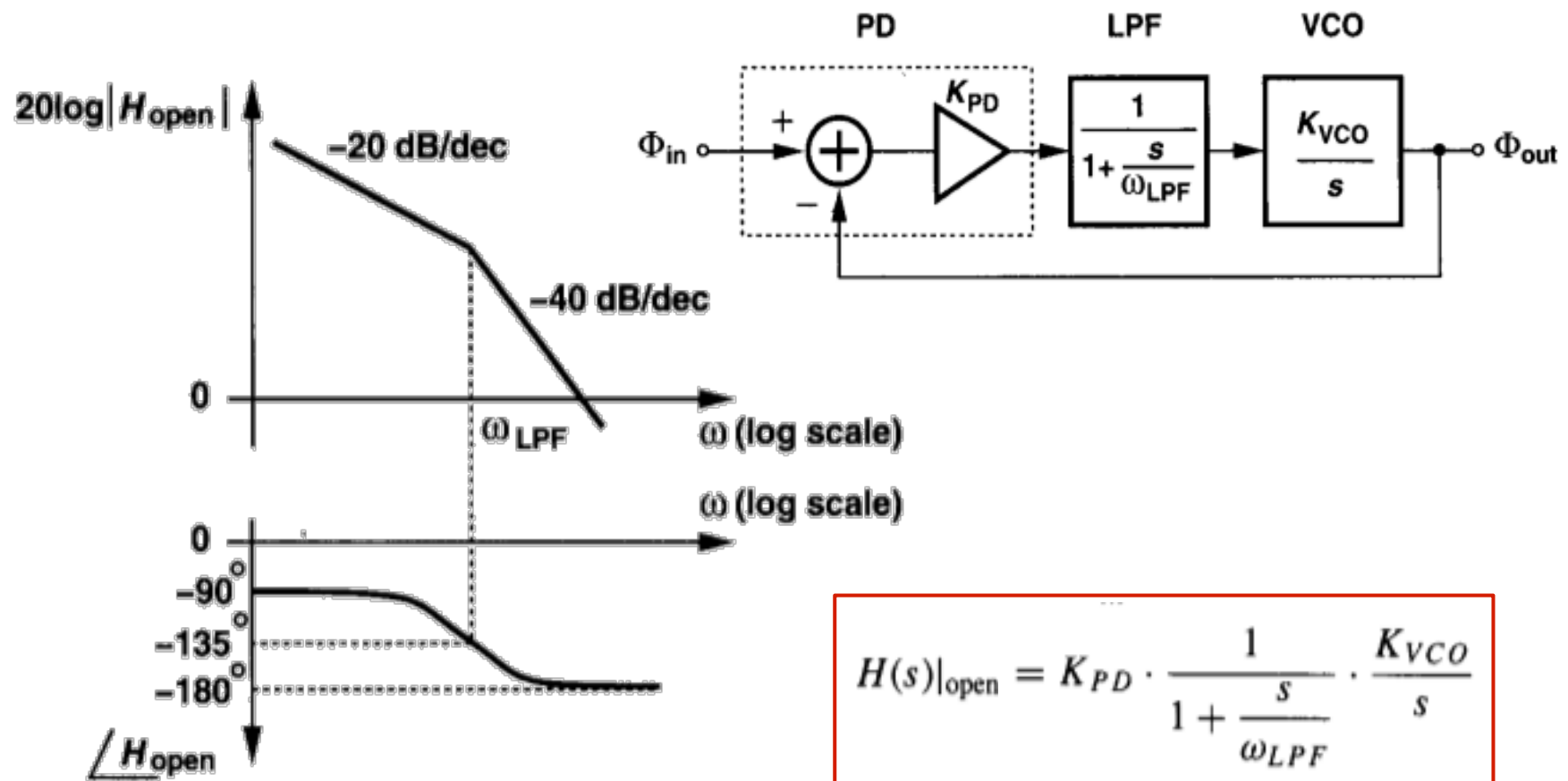
- ◆ For a preferred $\zeta \rightarrow \omega_n$ should be maximized for faster response

- ω_{LPF} and $K_{PD} K_{VCO}$ should be increased at the same time

- Strict trade-offs between response time, stability, steady-state ripple & jitter, and steady-state phase error

Loop Dynamics (V)

- ◆ From Bode plot of open-loop transfer function



- ◆ The loop becomes less stable if ...