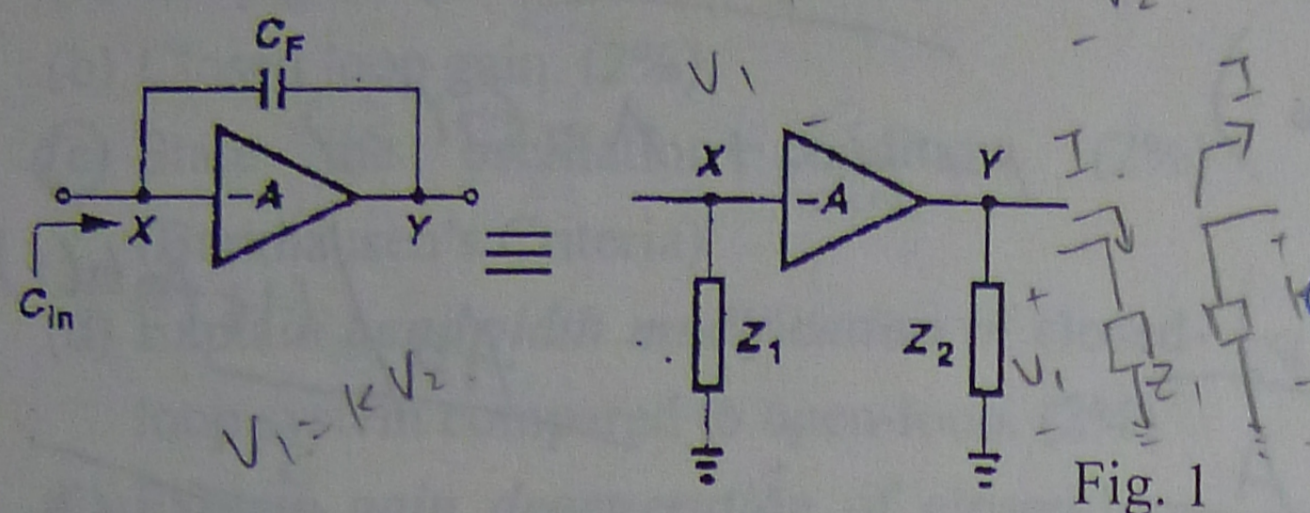


$$-kV_1 + V_1 = I$$

1. An amplifier with feedback capacitor C_F , open-loop gain $-A$, and equivalent circuit as shown in Fig. 1. Find Z_1 and Z_2 using Miller effect. (5%)



4. Assume there is a resistor with thermal noise = $4KTR$ (5%)

- (a) Draw two equivalent circuits of the resistor with noise voltage source and noise current source, respectively. (2.5%)
- (b) Sketch frequency response of the noise power spectral density (PSD v.s. f). (2.5%)

5. A R-C low-pass filter is shown in Fig. 5. The resistor's thermal noise = $4KTR$. Derive the total noise power at output node. (5%)

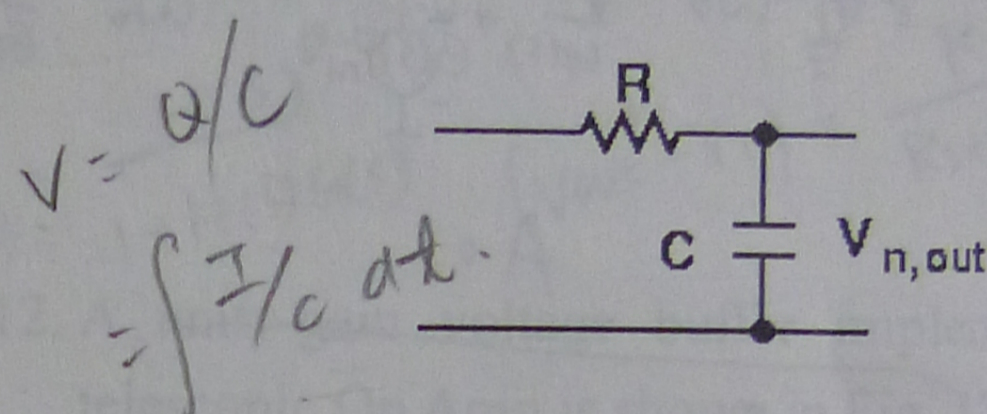


Fig. 5

2. A common source amplifier with C loading is shown in Fig. 2. (assume $r_o = \infty$, $|A_v| \gg 1$) (5%)

- (a) Use Miller effect to find the equivalent C_{in} at node X and C_{out} at node V_{out} . (2.5%)
- (b) Find the correlated input pole ω_{in} and output pole ω_{out} . (2.5%)

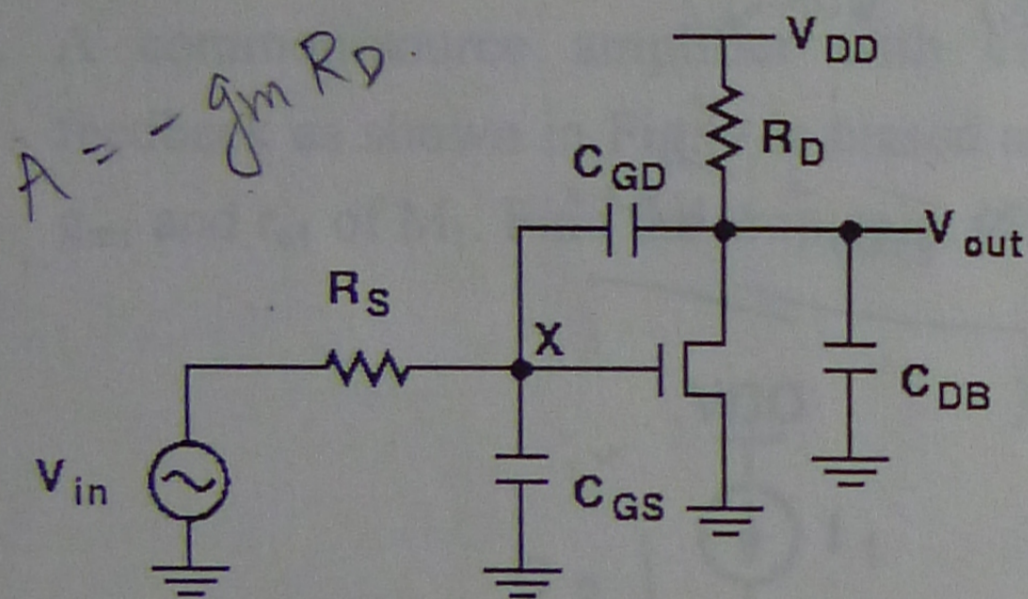


Fig. 2

6. A common source follower is shown in Fig. 6. The thermal noise and flicker noise of M_1 are $\overline{I_n^2} = 4kTg_m(\frac{2}{3})$ and $\overline{V_n^2} = \frac{K}{C_{ox}WL} \cdot \frac{1}{f}$. (10%)

- (a) Derive the input referred noise $\overline{V_{n,in}^2}$ due to thermal noise. (5%)
- (b) Derive the input referred noise $\overline{V_{n,in}^2}$ due to flicker noise. (5%)

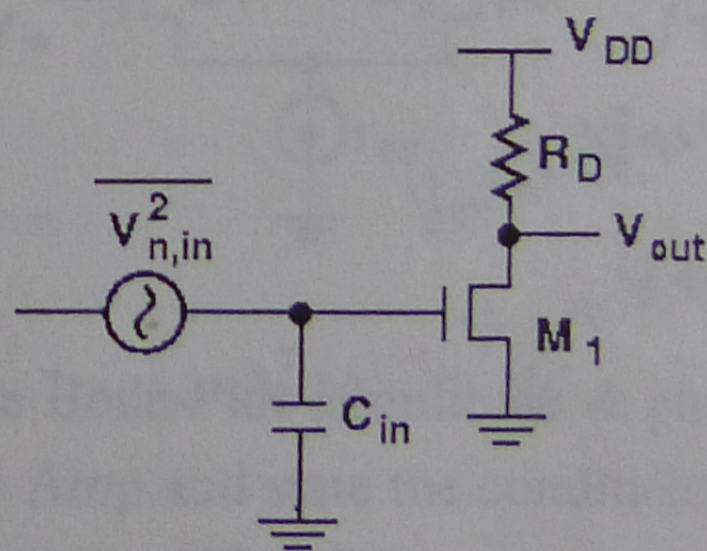
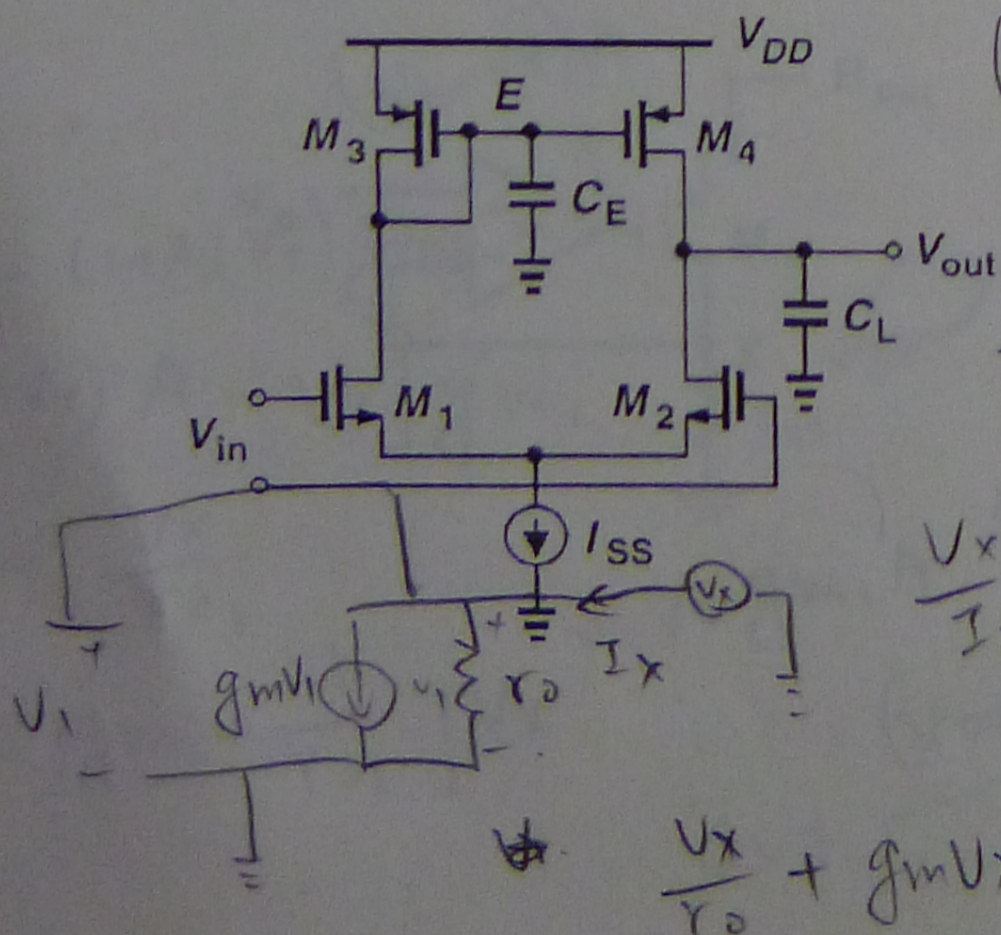


Fig. 6

3. A differential pair with capacitance loading is shown in Fig. 3 (5%)

- (a) Find the node of dominant pole and express it in terms of r_{ox} and C_x . (2.5%)
- (b) Find the node of second pole and express it in terms of g_{mx} , r_{ox} and C_x . (2.5%)



7. Explain the definitions and purposes of the following terminologies. (10%)

- (a) Common mode feedback. (2%)
- (b) Noise power spectrum density. (2%)
- (c) Flicker noise in MOS device. (2%)
- (d) Slewing in an Op Amp. (2%)
- (e) Phase margin. (2%)

8. A general block diagram of feedback system is shown in Fig. 8. Assume $H(s) = A_0/[1+(s/\omega_0)]$, answer the following definitions of terminology. (10%)

- (a) Loop gain. (2%)
- (b) Closed loop gain. (2%)
- (c) State the oscillation condition. (2%)
(Barkhausen's Criteria)
- (d) Explain *bandwidth modification* of closed-loop system compared to open-loop. (2%)
- (e) Explain *gain degeneration* of closed-loop system compared to open-loop. (2%)

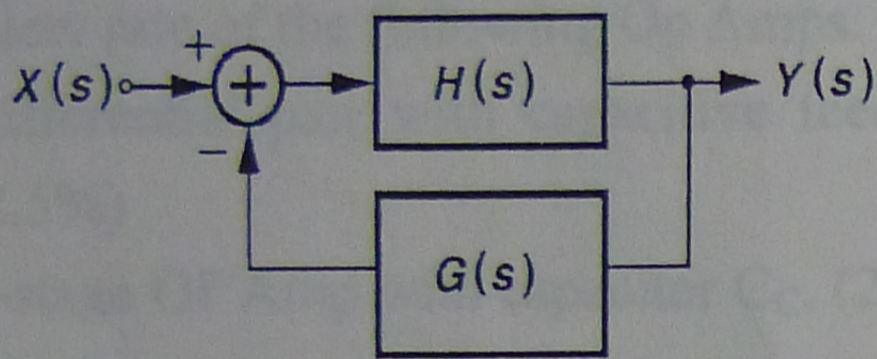


Fig. 8

11. A common-source amplifier with resistive feedback as shown in Fig. 11 is biased with g_{m1} and r_{o1} of M_1 . (10%)

- (a) Find the feedback factor. (2%)
- (b) Find the open-loop gain with loading effect. (4%)
- (c) Find the closed-loop gain V_{out}/V_{in} . (4%)

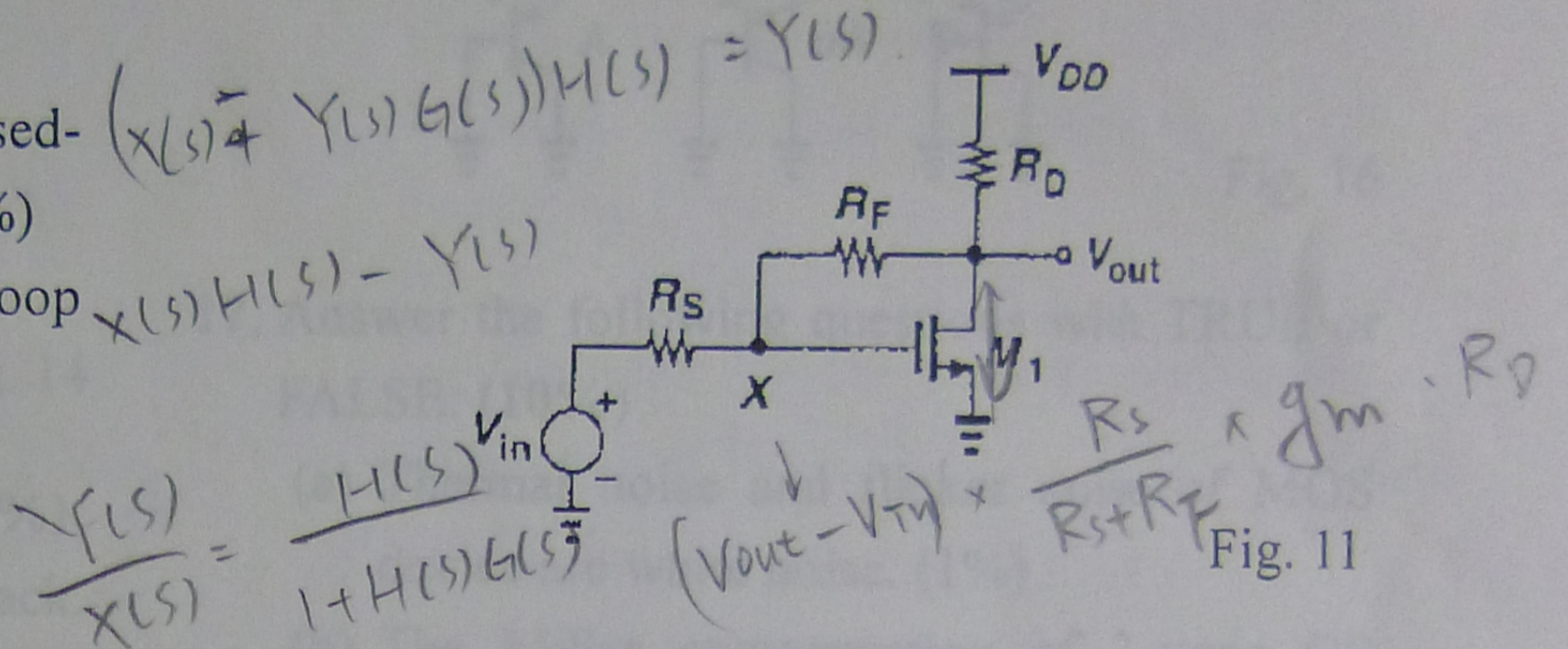


Fig. 11

12. A unity-gain voltage buffer implemented by telescopic Op Amp is shown in Fig. 12. Find the maximum output voltage swing. (5%)

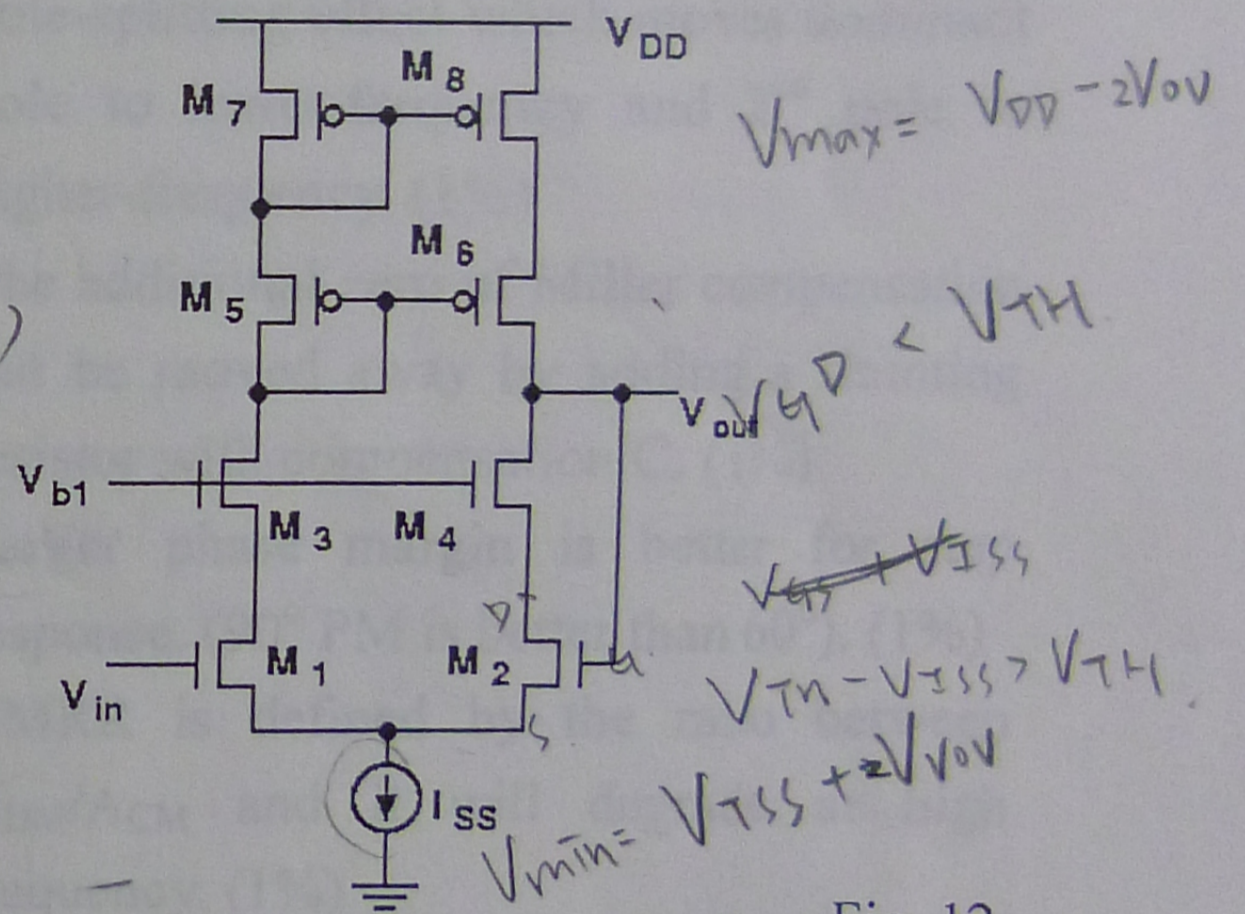


Fig. 12

9. A common-source amplifier with capacitive feedback as shown in Fig. 9 is biased at I_1 with g_{m1} and r_{o1} of M_1 . Find the loop gain. (5%)

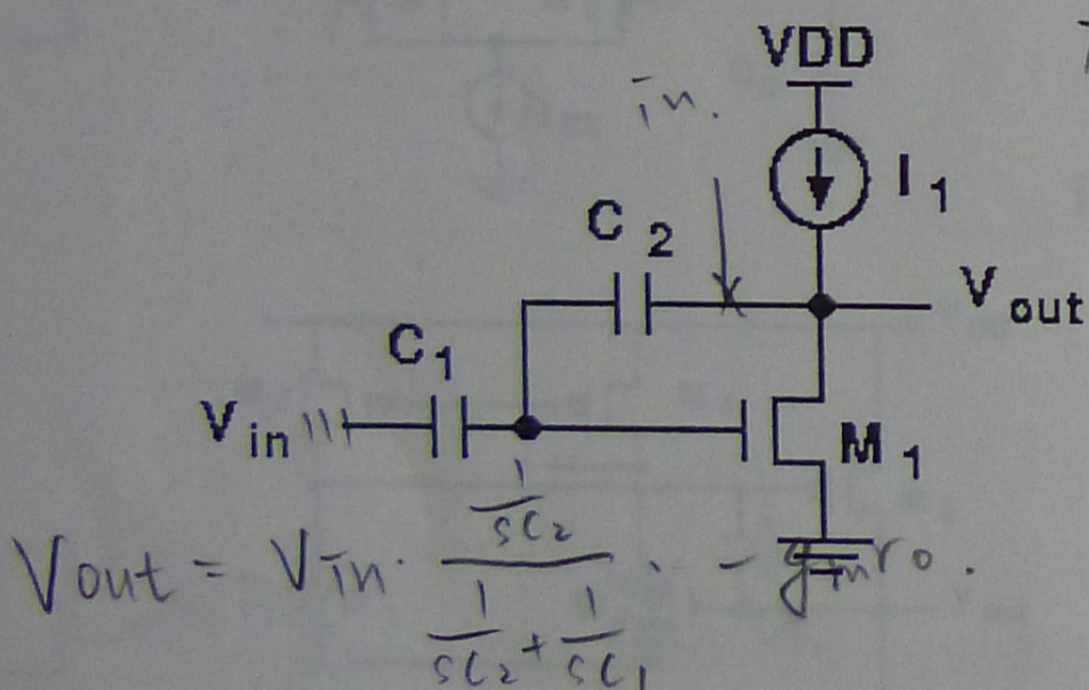


Fig. 9

10. An impedance boosting circuit is as shown in Fig. 10 with g_{m2} and r_{o2} of M_2 , find the R_{out} in term of r_{ox} , g_{mx} and A . (5%)

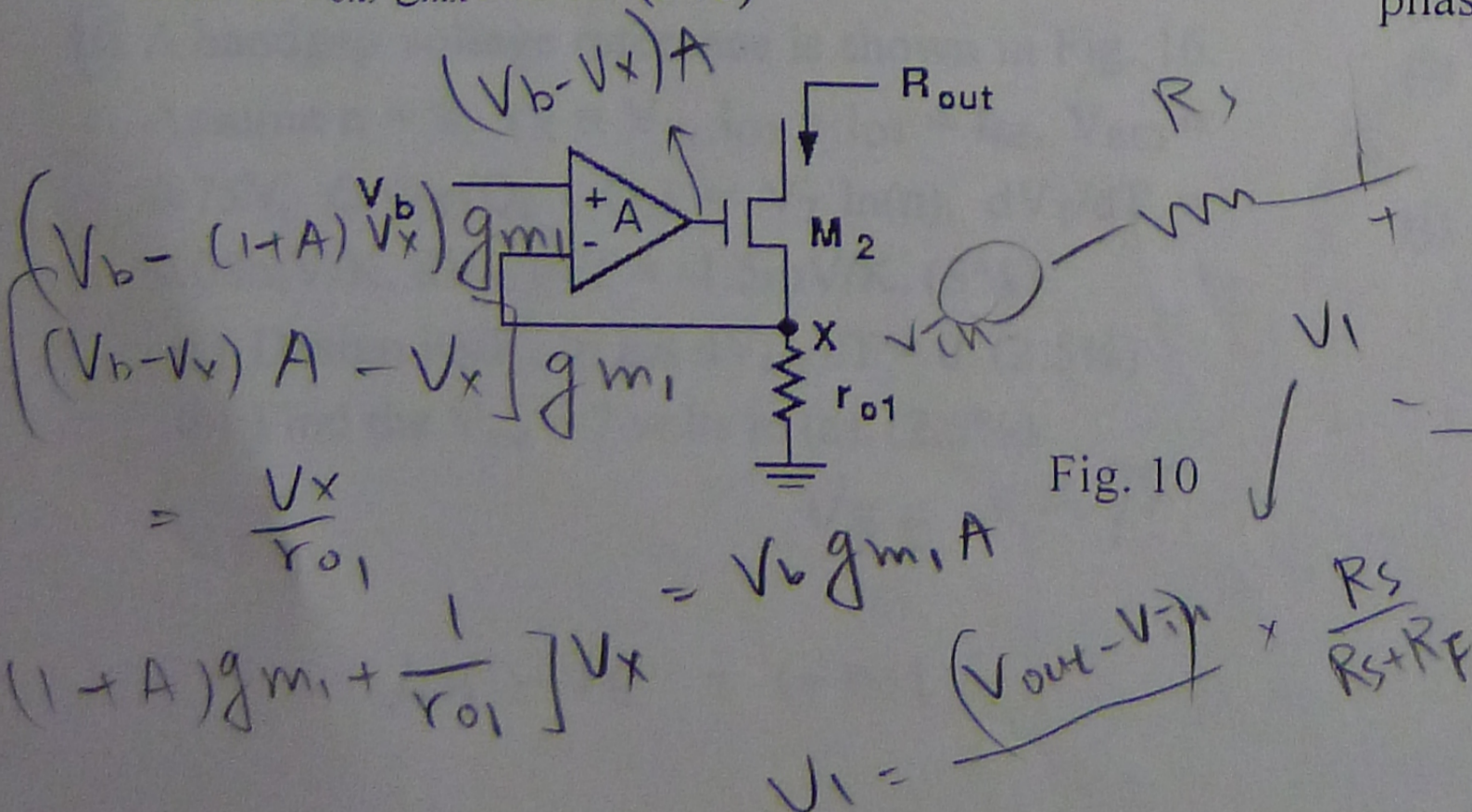
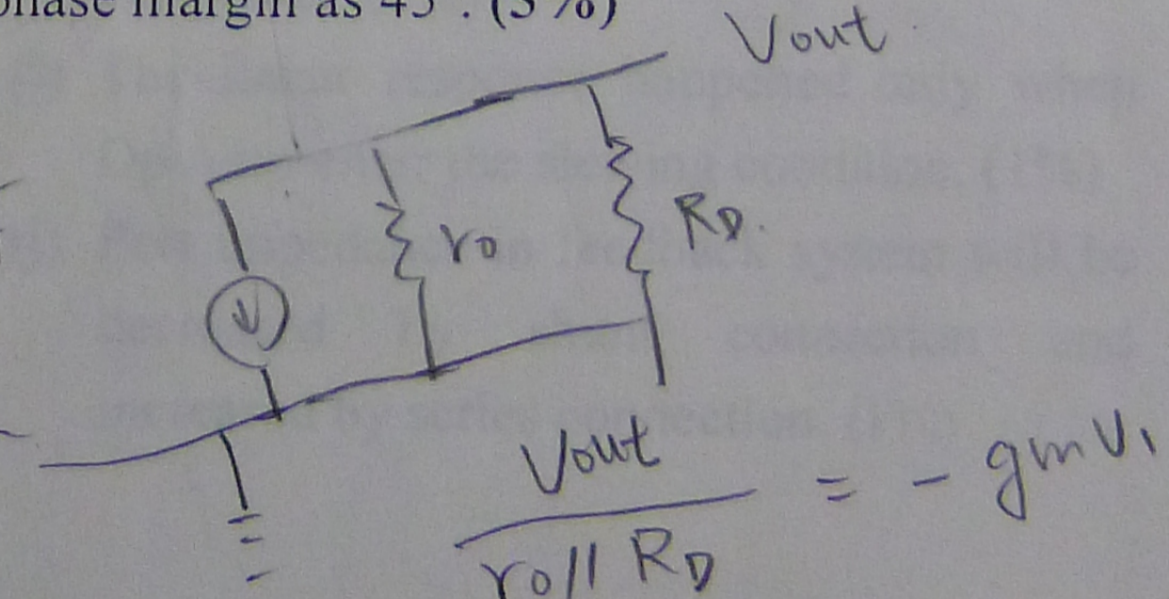
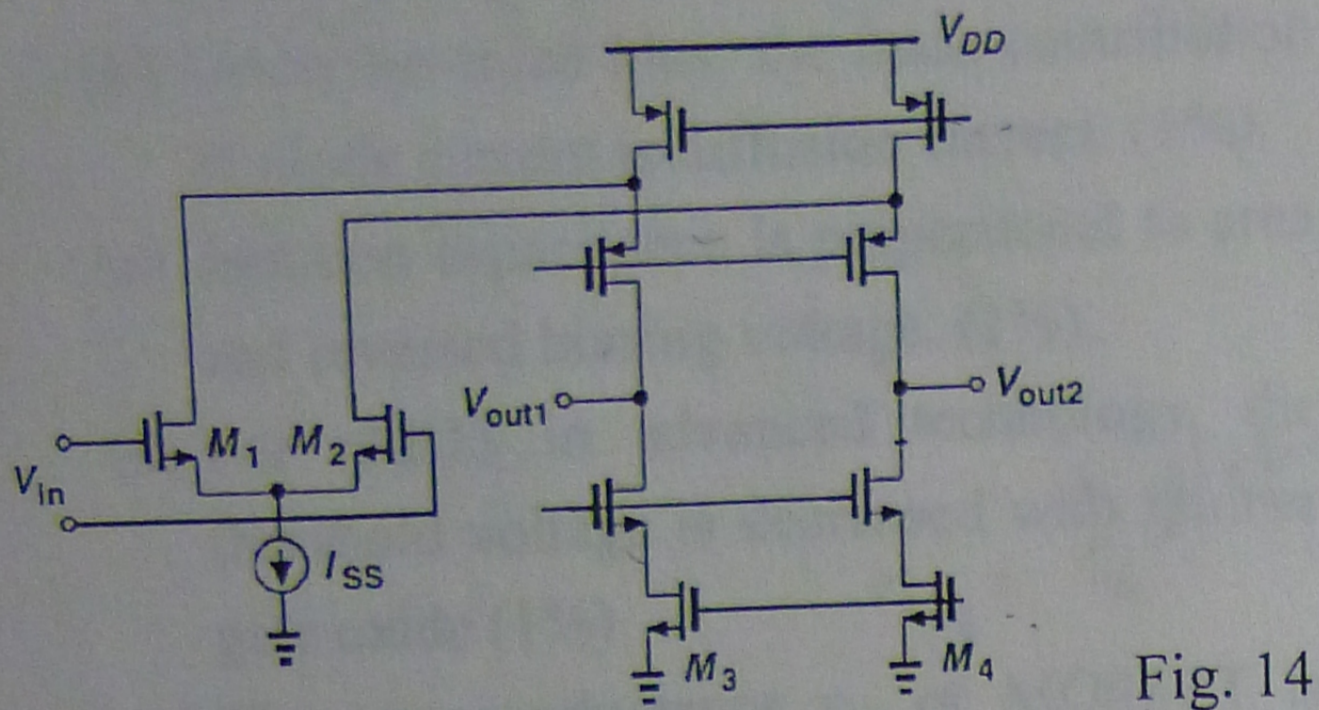


Fig. 10

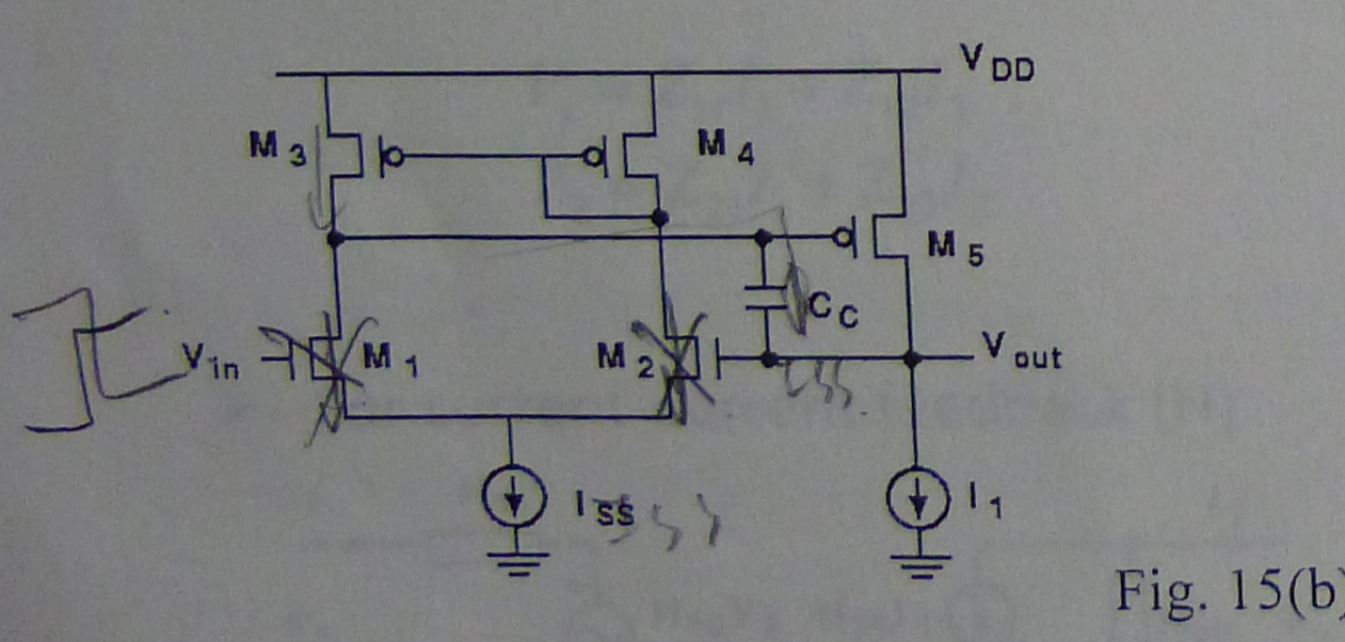
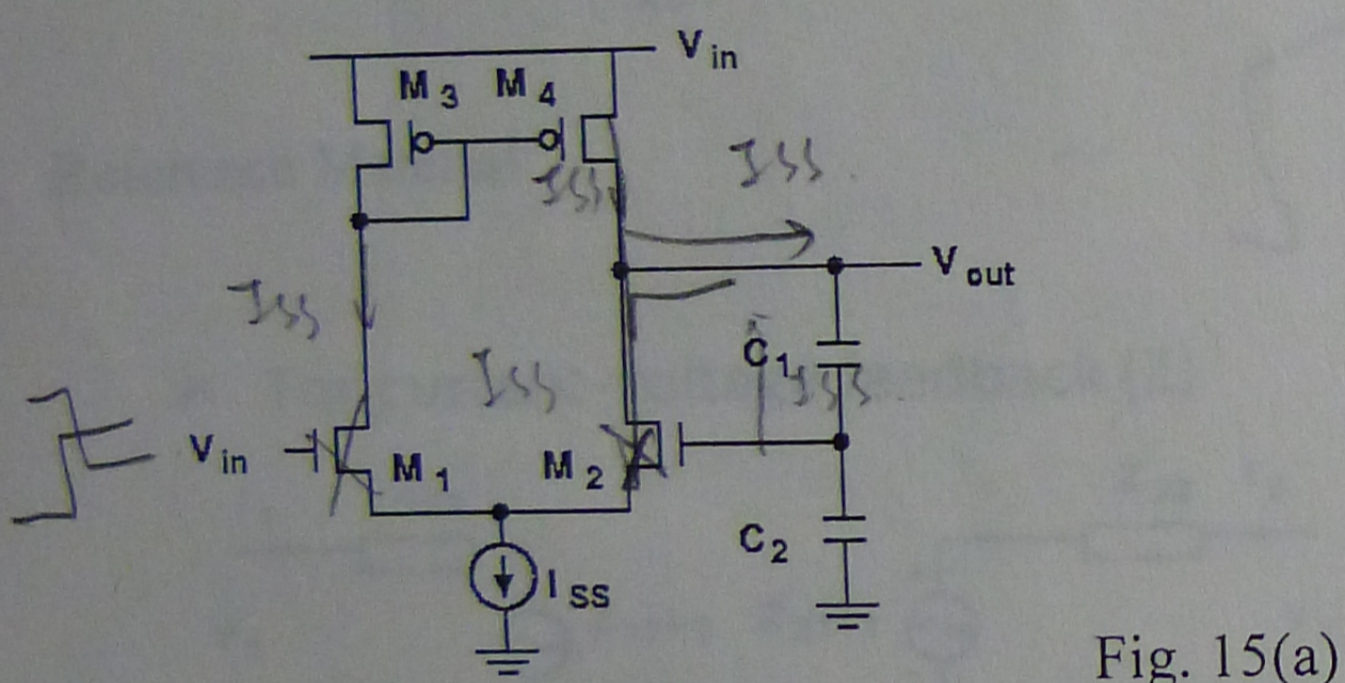
13. Sketch the Bode-Plot (amplitude & phase) of a 2-pole Op Amp and state the conditions to get a phase margin as 45° . (5%)



14. A fully-differential amplifier is shown in Fig. 14. Add necessary biases and the common-mode feedback circuit on it, sketch the complete circuit. (5%)



15. Find slew rate of the following Op Amps. (5%)
 (a) Differential pair with capacitive feedback. (2.5%)
 (b) 2-stage OP Amp with capacitor C_C. (2.5%)



16. A bandgap voltage reference is shown in Fig. 16. Assume $n = 8$, $V_X = V_Y$, $I_{D3} = I_{D4} = I_{D5}$, $V_{BE3} = 0.75V$, $\Delta V_{BE}(Q_1 - Q_2) = V_T \ln(n)$, $dV_T/dT = 0.08mV/K$, $dV_{BE3}/dT = -1.5mV/K$. (5%)

(a) Design R_2/R_1 to get $dV_{out}/dT = 0$. (2.5%)
 (b) Find the $V_{out} = ?$ volts in (a). (2.5%)

$V_{BE} = 0.75$

$V_{out} - V_E = \text{const}$

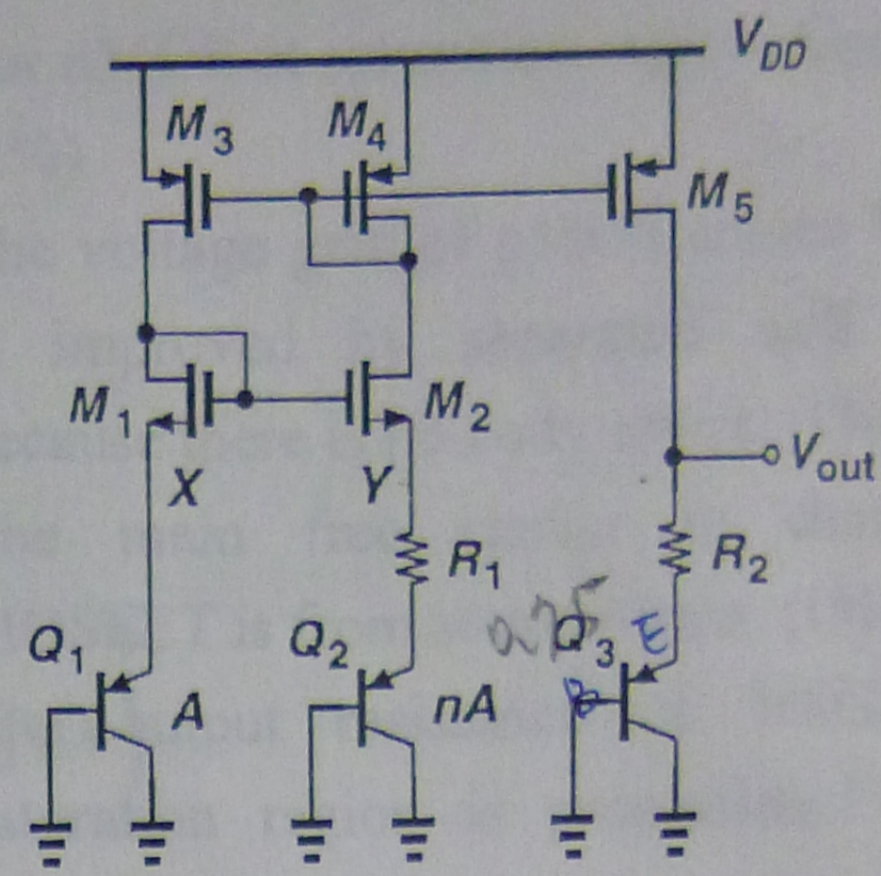


Fig. 16

17. Answer the following questions with TRUE or FALSE: (10%)

- (a) Thermal noise and flicker noise of MOS device are white noise. (1%)
- (b) The Miller compensation of 2-stage OP AMP is to make the dominant pole located at output node. (1%)
- (c) Miller compensation will result in a pole-splitting effect which moves dominant pole to lower-frequency and 2nd pole to higher-frequency. (1%)
- (d) The additional zero of Miller compensation can be moved away by adding a shunting resistor with compensation C. (1%)
- (e) Larger phase margin is better for step response. (90° PM is better than 60°). (1%)
- (f) CMRR is defined by the ratio between A_{DM}/A_{CM} and it will degrade at high frequency. (1%)
- (g) Usually the noise types in a circuit are from device and environmental noise. (1%)
- (h) Most of the noise sources in circuits are correlated. (1%)
- (i) The linear response happened only when Op Amp enter the slewing condition. (1%)
- (j) Port impedance in feedback system will be decreased by shunt connection and increased by series connection. (1%)

18. Answer the following questions with TRUE or FALSE: (10%)

- (a) Silicide is used to decrease the sheet resistance of layers in IC process. (1%)
- (b) Under reversed bias, the main contribution of diode current is diffusion current. (1%)
- (c) Junction capacitance is proportional to area and reversed biasing voltage. (1%)
- (d) For nMOS in advanced technology, the threshold voltage is decreased with thinner gate oxide (1%)
- (e) The transconductance g_m of MOSFET is proportional to bias current I_D at fixed W/L dimension. (1%)

- (f) For nMOS at saturation region, $C_{GS} > C_{GD}$. (1%)
- (g) The voltage gain of pMOS source follower is improved by separated well design, because there is no body effect. (1%)
- (h) The main free carrier in channel of MOSFET is from source/drain. (1%)
- (i) The output resistance of MOSFET at saturation region is proportional to bias current I_D . (1%)
- (j) PTAT current source is usually implemented by the positive temperature coefficient of V_{BE} . (1%)

Handwritten notes and equations:

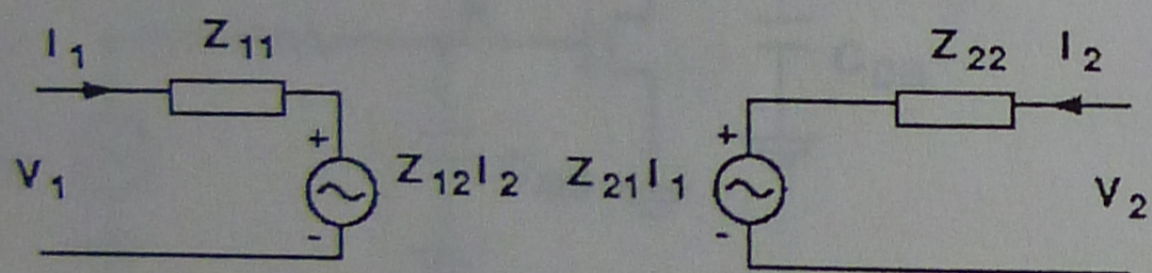
$$g_m = \frac{\partial I_D}{\partial V_{GS}} = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})$$

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$

$$V_x = V \times \frac{C_B}{C_{ox} + C_B} = V \times \frac{C_{ox}}{C_{ox} + C_B}$$

Reference Material

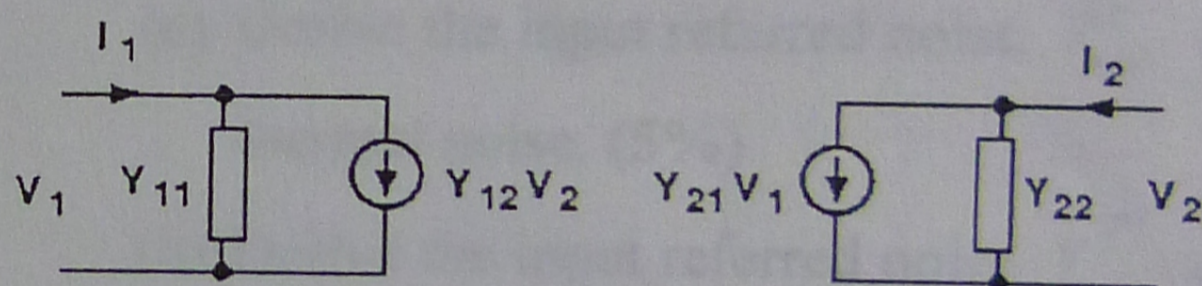
➤ For current-voltage feedback (Z)



$$V_1 = Z_{11}I_1 + Z_{12}I_2$$

$$V_2 = Z_{21}I_1 + Z_{22}I_2$$

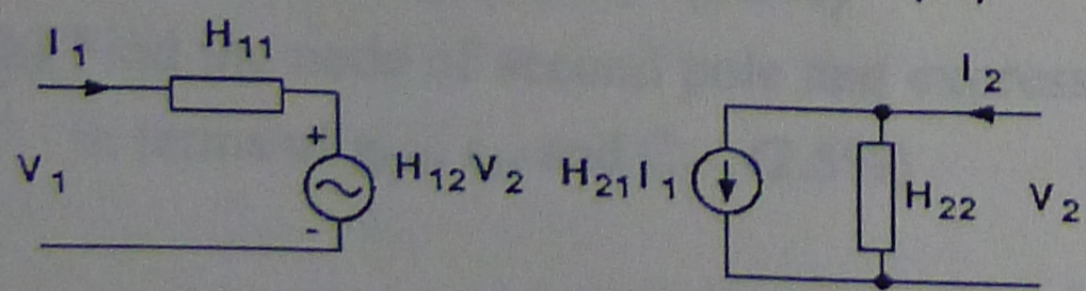
➤ For voltage-current feedback (Y)



$$I_1 = Y_{11}V_1 + Y_{12}V_2$$

$$I_2 = Y_{21}V_1 + Y_{22}V_2$$

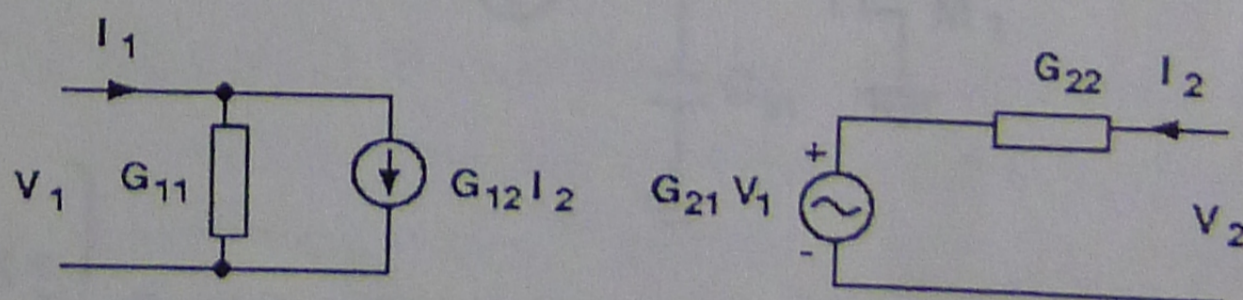
➤ For current-current feedback (H)



$$V_1 = H_{11}I_1 + H_{12}V_2$$

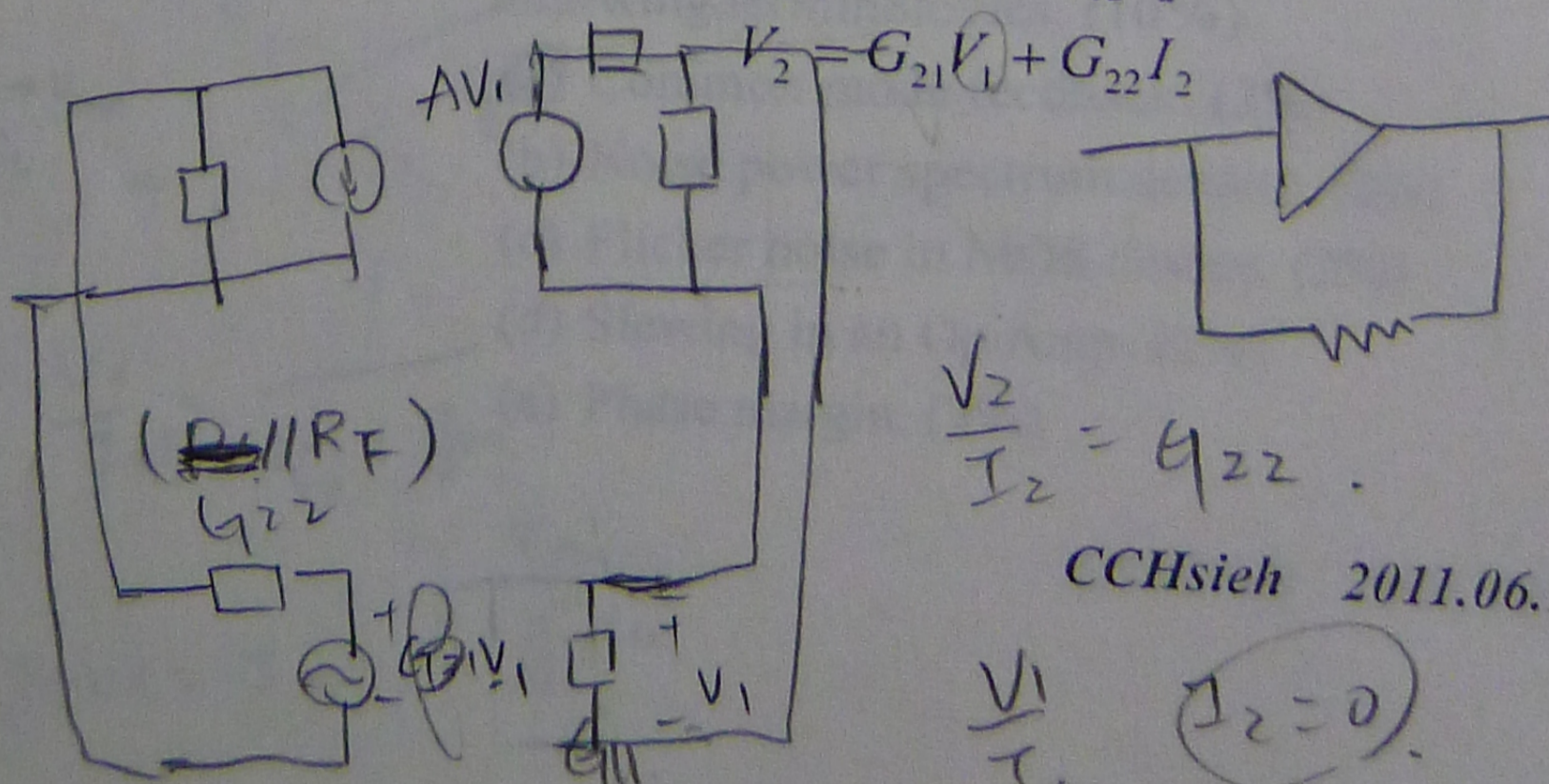
$$I_2 = H_{21}I_1 + H_{22}V_2$$

➤ For voltage-voltage feedback (G)



$$I_1 = G_{11}V_1 + G_{12}I_2$$

$$V_2 = G_{21}V_1 + G_{22}I_2$$



CCHsieh 2011.06.16