Sinusoidal Steady State Filters and Resonance

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Back to RC Network







$$V_{c} = \mathbf{V}_{i} \frac{Z_{C}}{Z_{C} + R} = \mathbf{V}_{i} \frac{\overline{j\omega C}}{\frac{1}{j\omega C} + R} \qquad \Rightarrow \quad \mathbf{V}_{c} = \frac{1}{1 + j\omega RC} \mathbf{V}_{i}$$

Transfer Function





Magnitude and Phase plots, A low pass filter.



Bode Plot



- **Transfer function** $H(j\omega) = \frac{\mathbf{V_c}}{\mathbf{V_i}} = \frac{1}{1 + j\omega RC}$
- **Bode Plot** for a transfer function assuming $RC = 2\pi \times 100$ rad/sec.



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Quick Review of Impedances





• Example2: $I_{ab} + R_{ab} + R_{ab} = R_{1} + j\omega L_{i}$ $j\omega L + R_{ab} = R_{ab} = R_{1} + j\omega L_{i}$ $J = R_{ab} =$

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Quick Review of Impedances



Example3:



RCL Impedances



RLC impedances as a function of frequency:



Filters built by Combining Impedances

Filters can be built by Combining Impedances :



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Series RLC





Transfer Function



$$\frac{\mathbf{V_r}}{\mathbf{V_i}} = \frac{j\omega CR}{-\omega^2 LC + 1 + j\omega CR}$$

Let's study this transfer function



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$$\frac{\mathbf{V_r}}{\mathbf{V_i}} = \frac{j\omega CR}{(1 - \omega^2 LC) + j\omega CR} = \frac{j\omega CR}{(1 - \omega^2 LC) + j\omega CR} \cdot \frac{(1 - \omega^2 LC) - j\omega CR}{(1 - \omega^2 LC) - j\omega CR}$$

$$\left|\frac{\mathbf{V_r}}{|\mathbf{V_i}|}\right| = \frac{V_r}{V_i} = \frac{\omega CR}{\sqrt{(1 - \omega^2 LC)^2 + (\omega CR)^2}} \qquad \text{Low } \omega: \quad \frac{V_r}{V_i} \approx \omega CR$$

High $\omega: \quad \frac{V_r}{V_i} \approx \frac{R}{\omega L}$
 $\omega \sqrt{LC} = 1: \frac{V_r}{V_i} = 1$

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What about?

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AM Radio Receiver





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AM Radio Receiver





Selectivity: Look at series RLC in more detail







• To find quality factor
$$Q = \frac{\omega_0}{\Delta \omega}$$

• We need to find
$$\omega_0$$
 and $\Delta \omega = ?$

Recall
$$\frac{\mathbf{V_r}}{\mathbf{V_i}} = \frac{R}{R + j\omega L + \frac{1}{j\omega C}} = \frac{1}{1 + j\left(\omega\frac{L}{R} - \frac{1}{\omega CR}\right)}$$

• At
$$\omega_0$$
, we have $\omega_0 \frac{L}{R} - \frac{1}{\omega_0 CR} = 0$

•
$$\omega_0$$
 is simply : $\omega_o = \frac{1}{\sqrt{LC}}$



• $\Delta \omega$ is the bandwidth, i.e. ω between magnitude fall to -3dB

• We need to find

$$\left|\frac{\mathbf{V_r}}{|\mathbf{V_i}|}\right| = \frac{V_r}{V_i} = \frac{1}{\sqrt{2}} = \left|\frac{1}{1+j\left(\omega\frac{L}{R} - \frac{1}{\omega CR}\right)}\right| = \left|\frac{1}{1\pm j}\right|$$
• That is $\omega\frac{L}{R} - \frac{1}{\omega CR} = \pm 1$

• Or
$$\omega^2 \mp \frac{R}{L}\omega - \frac{1}{LC} = 0$$

$$\omega_{1} = \frac{R}{2L} + \frac{1}{2}\sqrt{\frac{R^{2}}{L^{2}} + \frac{4}{LC}}$$

The roots of both equations are

 $\omega_2 = -\frac{R}{2L} + \frac{1}{2}\sqrt{\frac{R^2}{L^2} + \frac{4}{LC}}$

•
$$\Delta \omega$$
 is simply : $\Delta \omega = \omega_1 - \omega_2 = \frac{R}{L}$



Another way of looking at Q:

$$Q = 2\pi \frac{\text{EnergyStored}}{\text{Energylost per cycle}} = 2\pi \frac{\frac{1}{2}L|I_r|^2}{\frac{1}{2}R|I_r|^2\frac{2\pi}{\omega_0}} = \frac{\omega_0 L}{R}$$

• Q is simply :
$$Q = \frac{\omega_0}{\Delta \omega} = \frac{\omega_0}{R} = \frac{\omega_0 L}{R}$$
 $\omega_o = \frac{1}{\sqrt{LC}}$
• Q is simply : $Q = \frac{\omega_0 L}{R}$

• The quality factor
$$Q = \frac{\omega_0}{\Delta \omega}$$



Parallel RLC







• To find quality factor
$$Q = \frac{\omega_0}{\Delta \omega}$$

• We need to find
$$\omega_0$$
 and $\Delta \omega = ?$

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Recall
$$\frac{\mathbf{V}_{\mathbf{p}}}{\mathbf{I}_{\mathbf{0}}} = \frac{R}{1 + j\left(\omega CR - \frac{R}{\omega L}\right)}$$

• At
$$\omega_0$$
, we have $\omega_0 CR - \frac{R}{\omega_o L} = 0$

•
$$\omega_0$$
 is simply : $\omega_o = \frac{1}{\sqrt{LC}}$





• $\Delta \omega$ is the bandwidth, i.e. ω between magnitude fall to -3dB

• We need to find

$$\left|\frac{\mathbf{V_i}}{\mathbf{I_0}}\right| = \frac{V_i}{I_0} = \frac{R}{\sqrt{2}} = \left|\frac{R}{1 + j\left(\omega CR - \frac{R}{\omega L}\right)}\right| = \left|\frac{1}{1 \pm j}\right|$$
• That is $\omega CR - \frac{R}{\omega L} = \pm 1$

• Or
$$\omega^2 \mp \frac{1}{RC}\omega - \frac{1}{LC} = 0$$

$$\omega_1 = \frac{1}{2RC} + \frac{1}{2}\sqrt{\frac{1}{R^2C^2} + \frac{4}{LC}}$$

• The roots of both equations are $\omega_2 = -\frac{1}{2RC} + \frac{1}{2}\sqrt{\frac{1}{R^2C^2} + \frac{4}{LC}}$ • $\Delta\omega$ is simply : $\Delta\omega = \omega_1 - \omega_2 = \frac{1}{RC}$

Transfer Function





Example



- $L = 0.1 \text{ mH}, C = 1 \mu\text{F} \text{ and } R = 10 \Omega$
- Transfer function



$$Q = \frac{\omega_0}{2\alpha} = 1$$





Log scale







Linear scale



$$\omega_0 = \frac{1}{\sqrt{LC}} = 10^5 \text{ rad/s}$$

Transfer Function and Q



Transfer function

$$\frac{W_p}{I_0} = \frac{R}{1 + j\left(\omega CR - \frac{R}{\omega L}\right)}$$

Magnitude and Phase plots.



Revisit of the LPF with L



• $L = 20 \text{ mH}, C = 13 \text{ nF} \text{ and } R = 50 \Omega$



$$\alpha = \frac{1}{2RC} = 76.9 \times 10^4 \text{ rad/s} = 12.4\omega_0$$

$$Q = \frac{\omega_0}{2\alpha} = 24.8$$

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Time-domain Vs Frequency-domain



Power and Energy in an Impedance

- Power and energy are critical issues in the design of circuits.
- The power delivered to some arbitrary impedance Z = R + jX by a sinusoidal source. $v_i(t) = V_i \cos(\omega t + \phi)$

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Because power is not a linear function of v and i, we must be cautious about using impedance concepts in power calculations.

Time expressions



- Let's start with time expressions rather than complex amplitudes.
- The current and voltage as a function of time are.

$$i_i(t) = \operatorname{Re}(\mathbf{I}_i e^{j\omega t}) = \frac{V_i}{\sqrt{R^2 + X^2}} \cos(\omega t + \phi - \theta)$$
$$v_i(t) = V_i \cos(\omega t + \phi)$$

Then, the instantaneous power is given by:

$$p(t) = v_i i_i = \frac{V_i^2}{\sqrt{R^2 + X^2}} \cos(\omega t + \phi) \cos(\omega t + \phi - \theta)$$
$$= \frac{1}{2} \frac{V_i^2}{\sqrt{R^2 + X^2}} [\cos(2\omega t + 2\phi - \theta) + \cos\theta]$$

The instantaneous power for sinusoidal drive has a sinusoidal component at twice the frequency of the input signal, and the DC component.

Average power



• Because the average value of $cos(2\omega t)$ is zero, the average power flowing into an arbitrary impedance is just the DC term of the expression below.

$$p(t) = \frac{1}{2} \frac{V_i^2}{\sqrt{R^2 + X^2}} [\cos(2\omega t + 2\phi - \theta) + \cos\theta]$$

The average power :

$$\overline{p} = \frac{1}{2} \frac{V_i^2}{\sqrt{R^2 + X^2}} \cos \theta$$
$$\overline{p} = \frac{1}{2} V_i I_i \cos \theta$$

- The average power in terms of complex amplitudes of voltages and currents is one-half the product of the two magnitudes multiplied by the cosine of the angle between them.
- The term $\cos\theta$ is often called **the power factor**.

Average power



The average power can also be written directly in terms of complex voltage and complex current.

$$\overline{p} = \frac{1}{2} \operatorname{Re}[\mathbf{V}_{i}\mathbf{I}_{i}^{*}] = \frac{1}{2} \operatorname{Re}[\mathbf{V}_{i}^{*}\mathbf{I}_{i}]$$

Where V_i^* is the complex conjugate of V_i . I_i^* is the complex conjugate of I_i .

Using this notation, 1/2 VI* is often called complex power, whence the real part of the complex power is the average power, the "real" power, and the imaginary part is called reactive power.

Pure Resistance



■ Assume that the impedance is a pure resistance *R*, that is, X = 0 and $\phi = 0$.

$$p(t) = \frac{1}{2} \frac{V_i^2}{\sqrt{R^2}} [\cos(2\omega t) + \cos 0] = \frac{V_i^2}{2R} [1 + \cos(2\omega t)]$$

The average power dissipated in the resistor is:

$$\overline{p} = \frac{V_i^2}{2R}$$

• This is exactly one half of the power delivered by the DC voltage of the same amplitude. V_i^2/R



Root-Mean-Square (rms) Voltage



The root-mean-square voltage, abbreviated rms, which is related to the peak amplitude of the sinewave by the square root of two.

$$V_{rms} = \frac{V_i}{\sqrt{2}}$$

In terms of the rms unit, average power is :

$$\overline{p} = \frac{V_i^2}{2R} = \frac{(V_{rms})^2}{R}$$

- For non-sinusoidal voltages, the general definition of rms voltage is, as the name implies, $V_{\rm rms} = \sqrt{\overline{v}^2(t)}$
- Thus, the 110-V AC power from a wall socket is 110 volts rms,
- Or $110 \times \sqrt{2} = 155.6$ volts peak.

Pure Reactance



• If the impedance consists only of inductor ($\theta = \pi/2$), that is, R = 0. Also assume that $\phi = 0$.

$$p(t) = \frac{V_i^2}{2X} [\cos(2\omega t - \frac{\pi}{2}) + \cos\frac{\pi}{2}] = \frac{V_i^2}{2X} \cos(2\omega t - \frac{\pi}{2}) = \frac{V_i^2}{2X} \sin(2\omega t)$$

• If the impedance consists only of capacitor ($\theta = -\pi/2$):

$$p(t) = \frac{V_i^2}{2X} \left[\cos(2\omega t + \frac{\pi}{2}) + \cos(-\frac{\pi}{2})\right] = \frac{V_i^2}{2X} \cos(2\omega t + \frac{\pi}{2}) = -\frac{V_i^2}{2X} \sin(2\omega t)$$

In both cases, the average power is zero.



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Pure Reactance



The L's and C's absorb power for two quarters of each cycle, and deliver the power back to the source during the other two quarter cycles.



- Power companies are not happy about this state of affairs, because they still must supply the power and pay for the power losses in the transmission line.
- Although there is no average power supplied to this lossless circuit in the sinusoidal steady state, there is energy stored on the average.

Average Stored Energies



For a capacitor, the stored energy is.

$$W_{C} = \frac{1}{2}Cv^{2}(t) = \frac{1}{2}C[V_{i}\cos(\omega t)]^{2} = \frac{1}{2}CV_{i}^{2}\left(\frac{1}{2} + \frac{1}{2}\cos(2\omega t)\right)$$

- Again a DC term and a double-frequency term.
- The average stored energy is

$$W_C = \frac{1}{2} C V_i^2 \left(\frac{1}{2}\right) = \frac{1}{4} C V_i^2$$

A similar derivation for an inductor yields:

$$\overline{W}_{L} = \frac{1}{4}LI_{i}^{2}$$
 where $i_{L}(t) = I_{i}\cos(\omega t)$

Example







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Peak Voltage in Resonant Circuit



- Assuming a cosine wave for the voltage source: $v_i(t) = V_i \cos \omega t$
- Assume that the circuit is being driven at its resonant frequency.



The voltage across either the capacitor or the inductor in a series resonant circuit is Q times the input voltage when the circuit is driven at its resonant frequency.

Stored Energy in Resonant Circuit

- Assuming a cosine wave for the voltage source: $v_i(t) = V_i \cos \omega t$
- The voltage across the capacitor is:

$$v_C(t) = \operatorname{Re}[\mathbf{V}_{\mathbf{c}}e^{j\omega_0 t}] = \operatorname{Re}[-jV_iQe^{j\omega_0 t}] = V_iQ\sin\omega t$$

- The energy stored in the capacitor $w_{C} = \frac{1}{2} C V_{i}^{2} Q^{2} \sin^{2}(\omega_{0} t)$ $= \frac{1}{2} C V_{i}^{2} Q^{2} [1 - \cos(2\omega_{0} t)]$
- The energy stored in the inductor

$$i_L(t) = \operatorname{Re}[\operatorname{I}e^{j\omega_0 t}] = \frac{V_i}{R} \cos \omega_0 t$$

$$w_{L} = \frac{1}{2}L\frac{V_{i}^{2}}{R^{2}}\cos^{2}(\omega_{0}t)$$
$$= \frac{1}{2}L\frac{V_{i}^{2}}{R^{2}}[1 + \cos(2\omega_{0}t)]$$

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Summary



- The performance of a resonant circuit is summarized by its frequency response. The frequency response comprises plots of magnitude and phase angle versus frequency.
- The magnitude plot is sketched by drawing the low-frequency and the high-frequency asymptotes. The two asymptotes intersect at the break frequency.
- The quality factor Q, the resonant frequency ω_0 , and the damping factor α are three key parameters that characterize the behavior of resonant systems.
- The average power in terms of complex amplitudes of voltages and currents is one-half the product of the two magnitudes multiplied by the cosine of the angle between them.
- The bandwidth is related to the resonant frequency by the quality factor:

$$Q = \frac{\text{Resonant frequency}}{\text{Bandwidth}}$$