
Lab 7: Single-Stage MOSFET Amplifiers

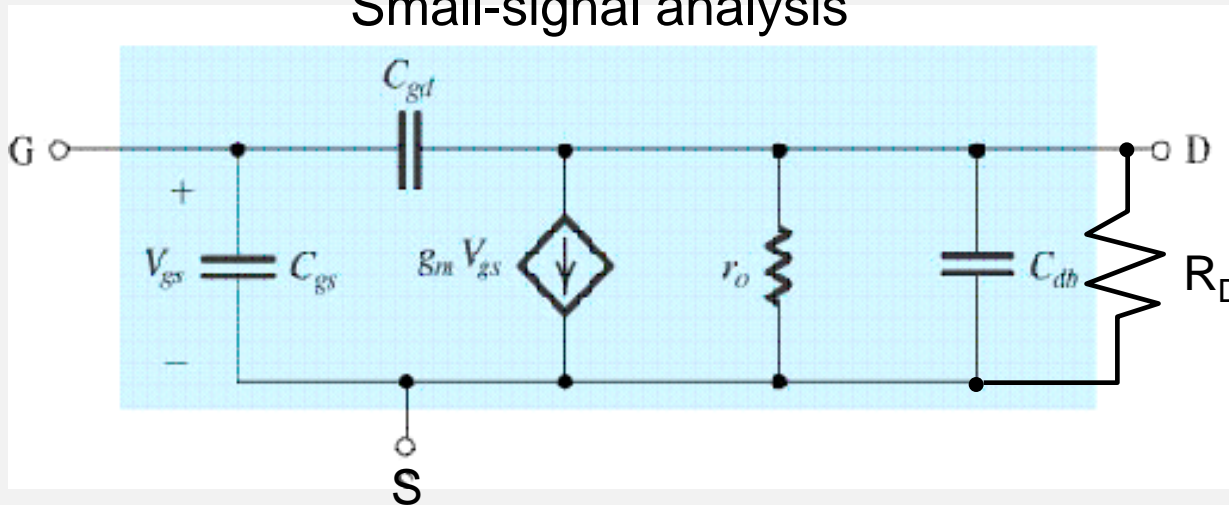
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Common-Source (CS) Amplifier

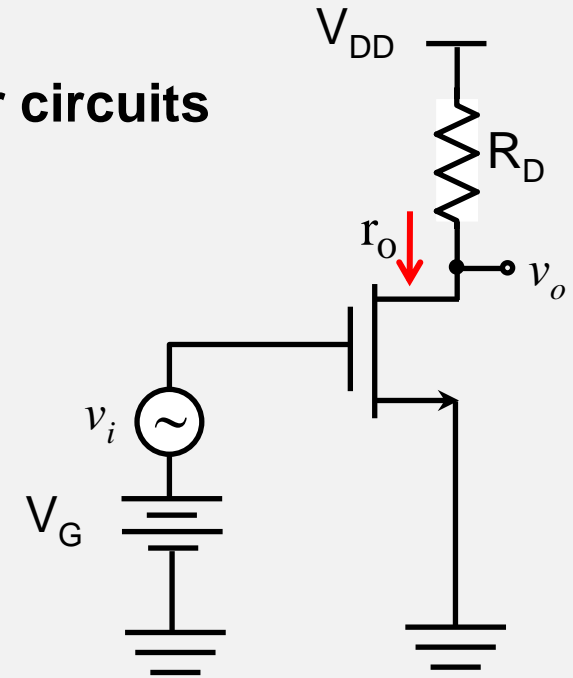
- Common-source amplifier
 - The most widely used of all MOSFET amplifier circuits
 - Suitable for gain stage
 - High input impedance
 - High output impedance

Small-signal analysis



Note: Make sure that $V_{ds} > V_{gs} - V_t$ for the transistor to operate in the saturation region

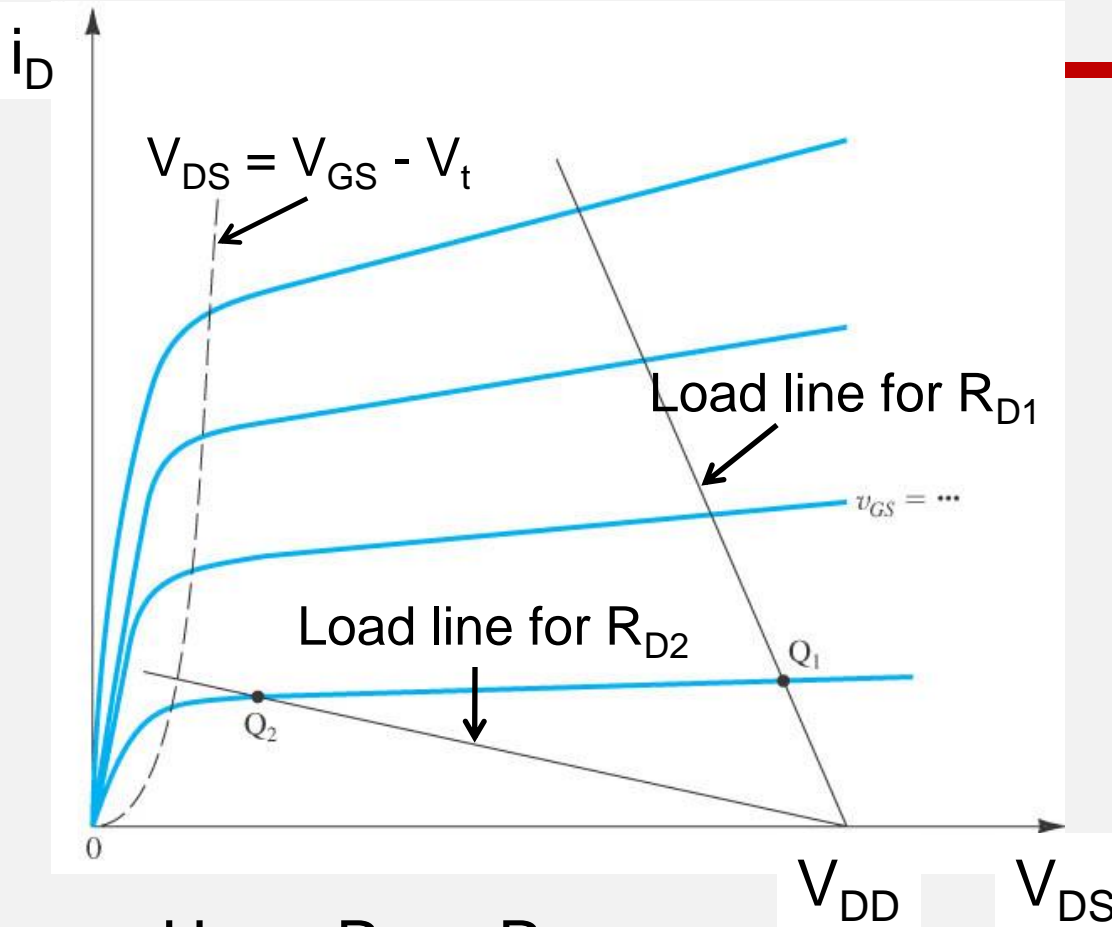
$$g_m = \mu_n C_{ox} \frac{W}{L} (V_{gs} - V_t) = \frac{2I_D}{V_{gs} - V_t}$$



$$v_o = -g_m v_i (r_o \parallel R_D)$$

$$\Rightarrow \frac{v_o}{v_i} = -g_m (r_o \parallel R_D)$$

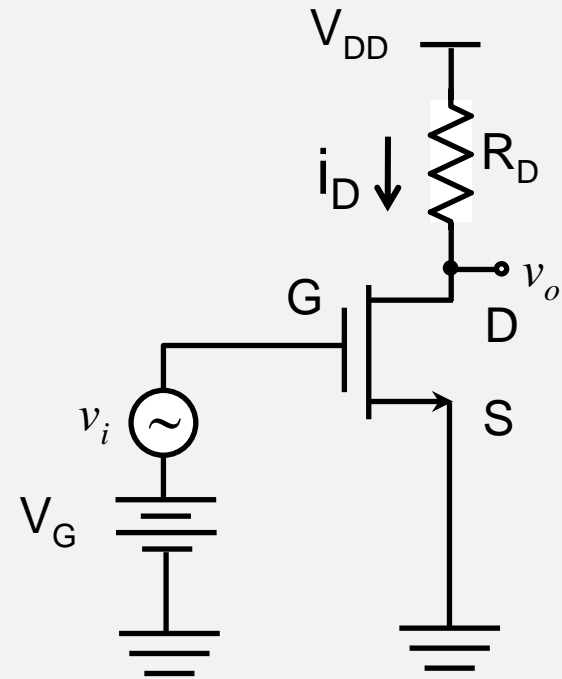
Output Signal Swing and Load Line



Here, $R_{D1} < R_{D2}$

Case 1: not enough "headroom"

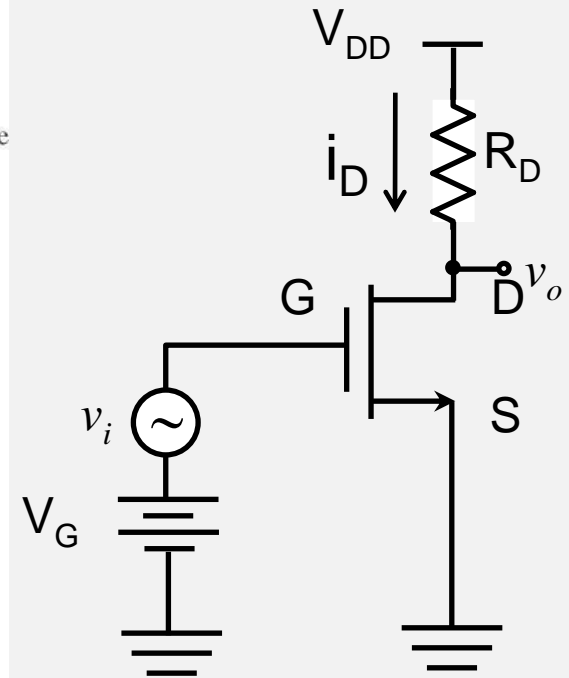
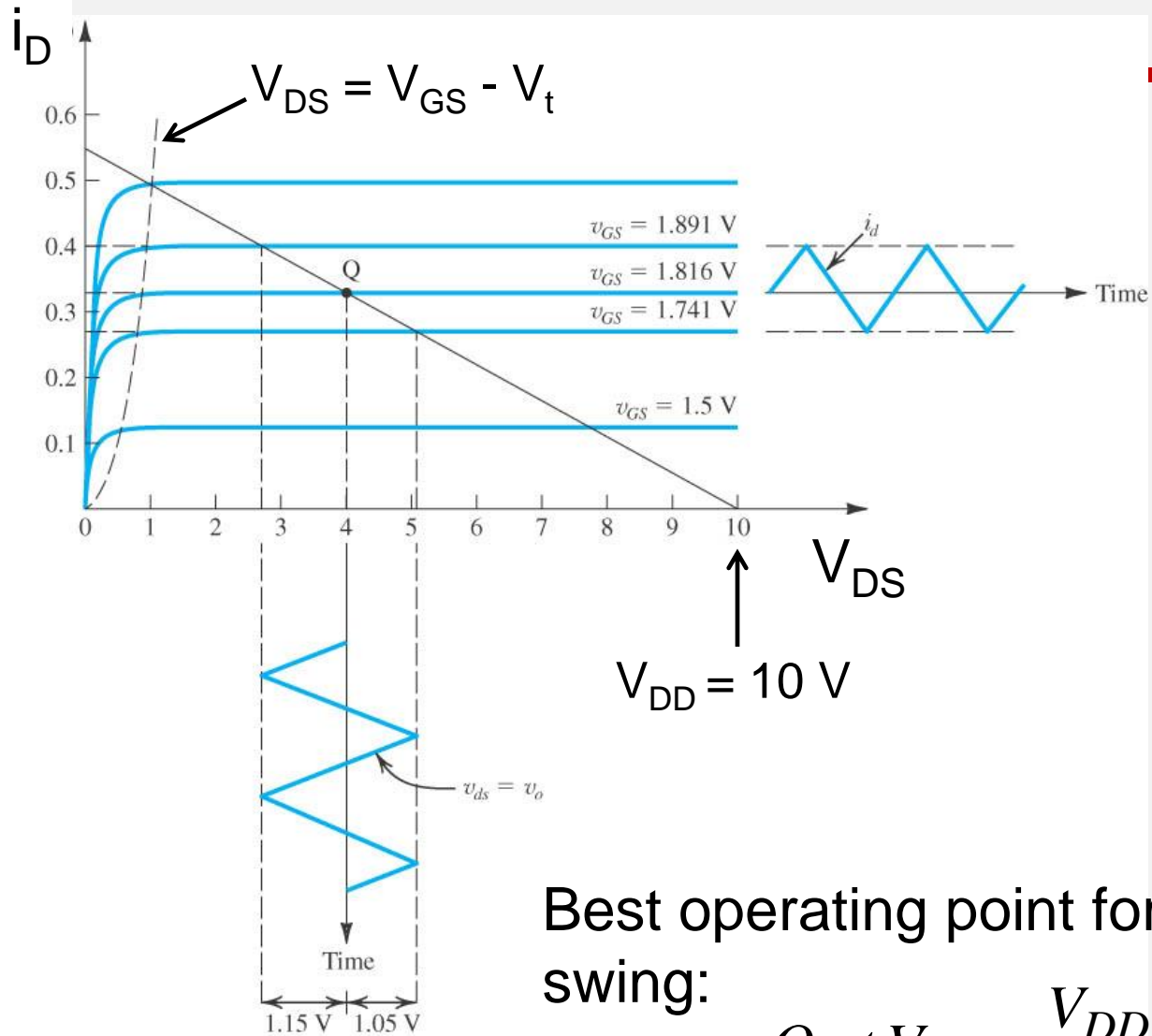
Case 2: not enough "legroom"



First, $v_o = V_{DS}$

$$\text{load line : } i_D = \frac{V_{DD} - v_o}{R_D}$$

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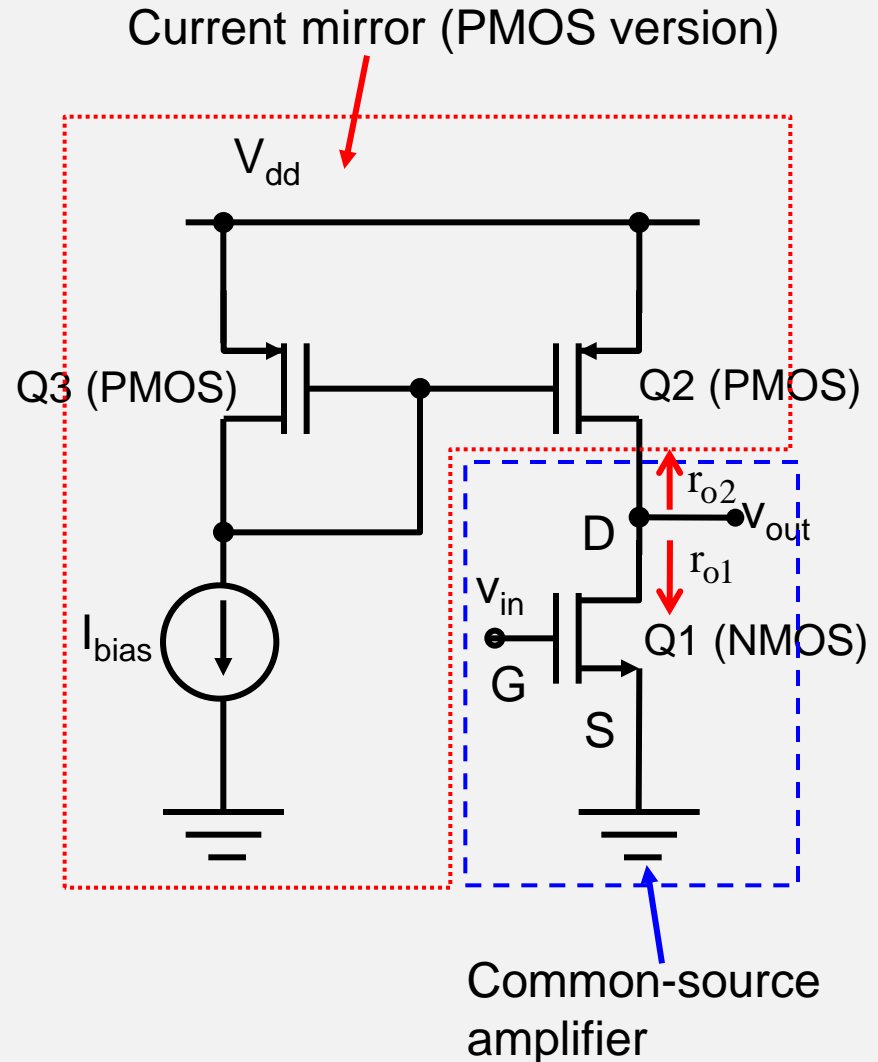
Best operating point for maximum swing:

(b) $Q \text{ at } V_{DS} \approx \frac{V_{DD}}{2} = 5 \text{ V}$

CS Amplifier with an Active Load

- A p-type current mirror provides the bias current and active load to a n-type common-source amplifier Q1
- Using small-signal analysis, the voltage gain:

$$A_v = \frac{V_{out}}{V_{in}} = -g_{m1}(r_{o1} // r_{o2})$$

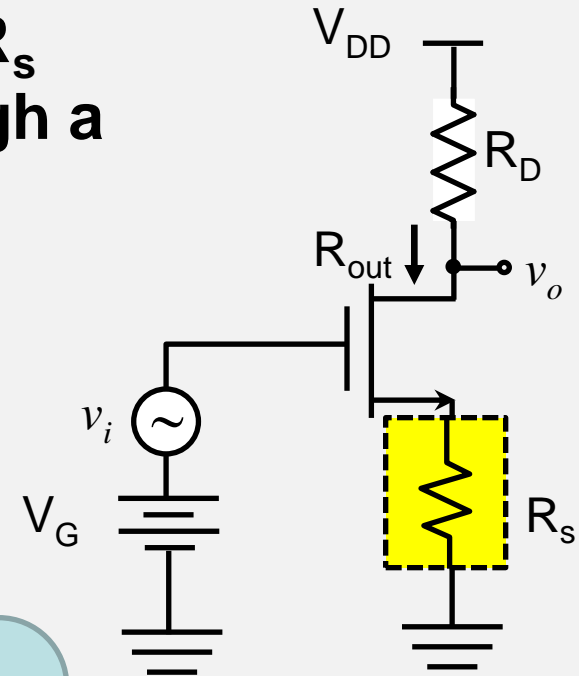
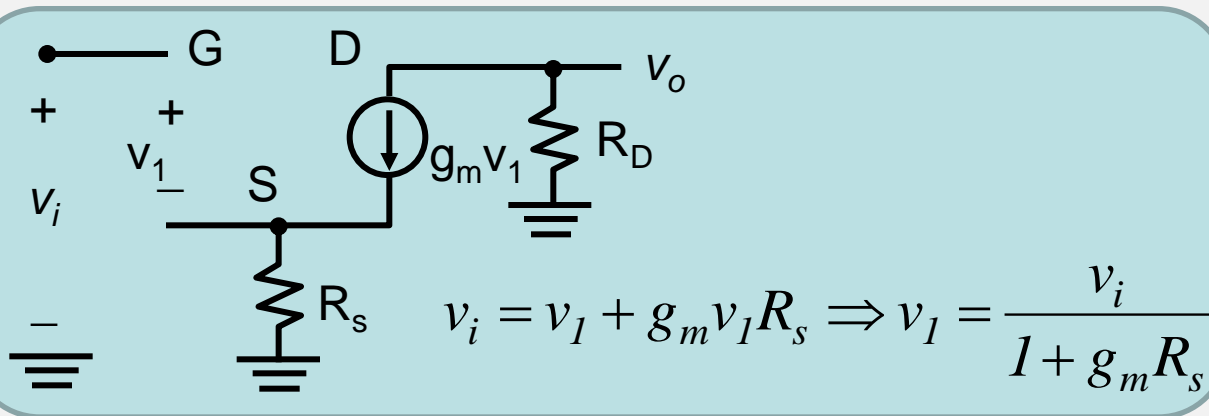


CS Amplifier with Source Degeneration

The source degeneration resistance R_s can stabilize the bias current I_D through a feedback mechanism (why?)

Gain reduces by a factor of $(1 + g_m R_s)$

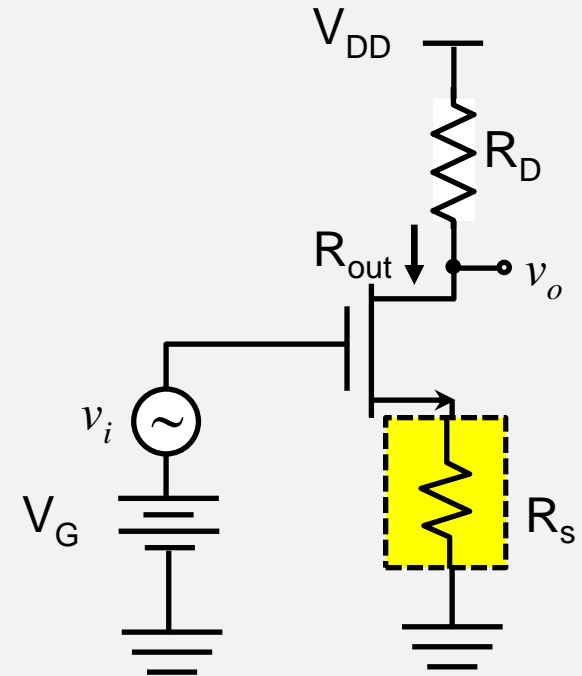
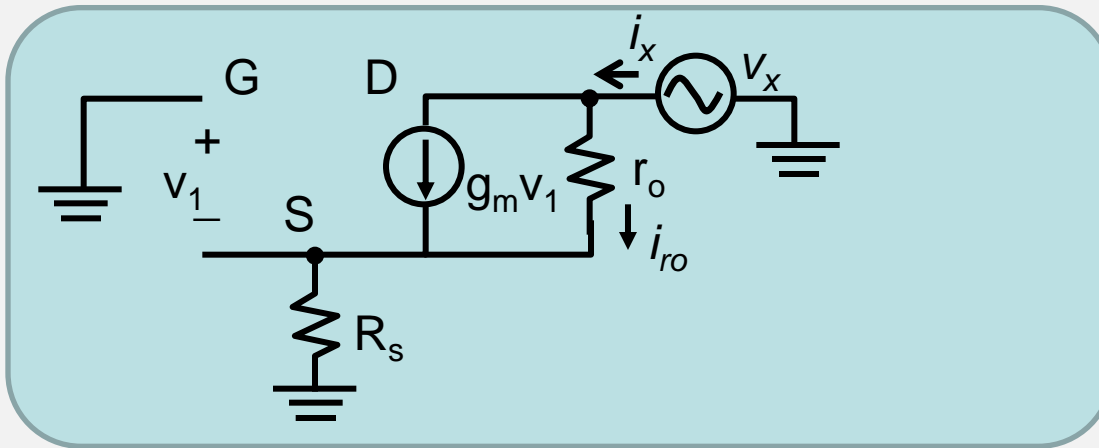
$$\frac{v_o}{v_i} \approx -\frac{g_m R_D}{1 + g_m R_s} \quad (\lambda = 0)$$



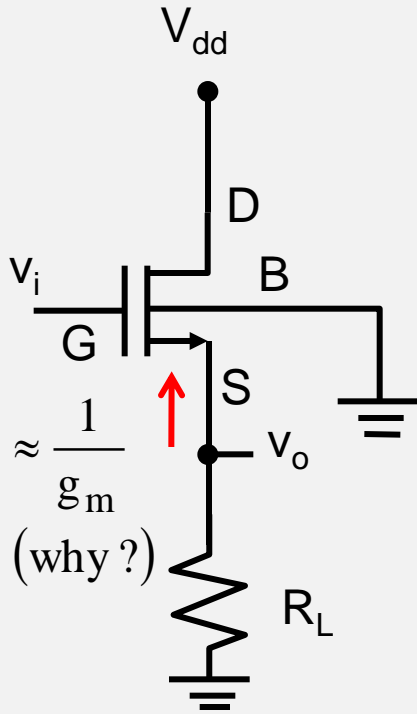
R_{out} of CS Amplifier with Source Degeneration

If $\lambda \neq 0$,
$$R_{out} = \frac{V_x}{i_x} = (1 + g_m r_o) \cdot R_s + r_o$$

same as that of the common-gate amplifier



Common-Drain (CD) Amplifier (Source Follower)

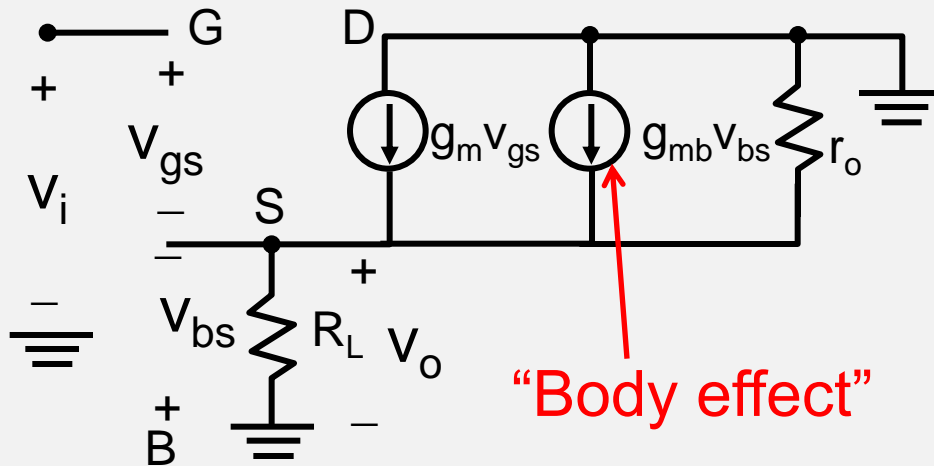


■ Characteristics:

- Voltage buffer amplifier with a gain close to 1
- High input impedance: most of the voltage drop of v_i occurs on the gate
- Low output impedance: most of the voltage drop occurs on R_L
- Used often as the output stage in a multi-stage amplifier

Small-Signal Analysis of CD Amplifier

- Small signal gain (without body effect)



$$v_o = g_m v_{gs} (r_o \parallel R_L) \quad (1)$$

$$v_i = v_{gs} + v_o \quad (2)$$

Solve (1) and (2):

$$\frac{v_o}{v_i} = \frac{R_L \parallel r_o}{(R_L \parallel r_o) + \frac{1}{g_m}} \approx 1$$

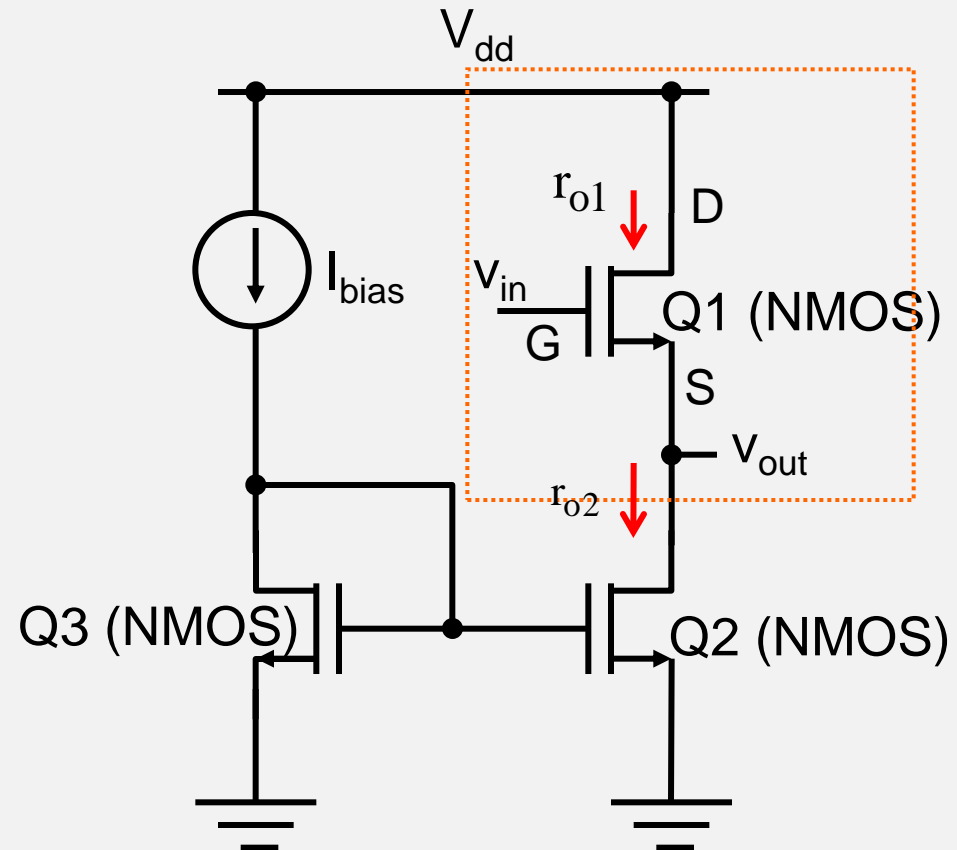
(for $R_L \parallel r_o \gg 1/g_m$)

“Body effect”: The threshold voltage increases when the source and the body terminals are not connected.

Source Follower with an Active Load

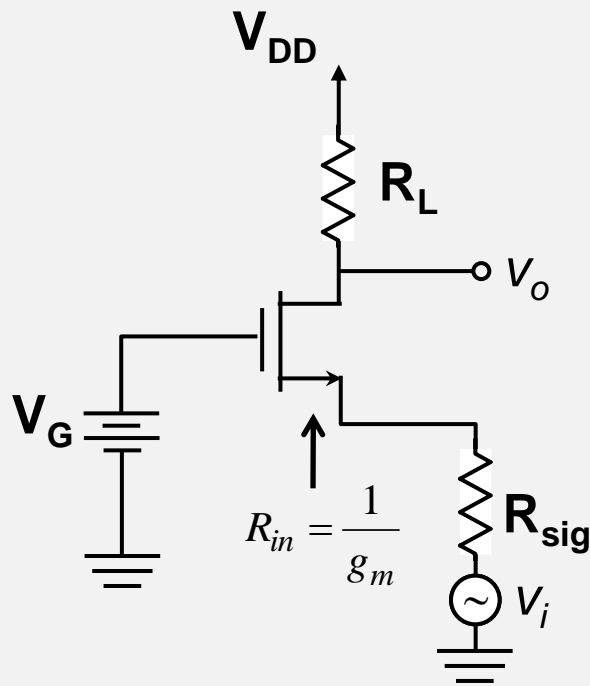
- Q1 is the source follower (a voltage buffer) with an active load implemented by a n-type current mirror

$$\frac{V_o}{V_i} = \frac{r_{o1} \parallel r_{o2}}{(r_{o1} \parallel r_{o2}) + \frac{1}{g_{m1}}}$$



Common-Gate (CG) Amplifier

- **Why uses a common-gate amplifier?**
 - It's a unity-gain current amplifier (current buffer) that reproduces the current in the drain terminal at a high output resistance
 - Can be used to make the cascode circuit



- **Compare a CG amplifier to a CS amplifier**
 - low input resistance
 - CG's overall voltage gain is smaller by a factor of about $1+g_m R_{sig}$
 - CG's gain is non-inverting
 - more influence by the body effect since the source cannot be connected to the body

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- Without channel-length modulation ($\lambda = 0$)

$$v_o = -g_m \cdot v_{gs} \cdot (R_L \parallel R_{out})$$

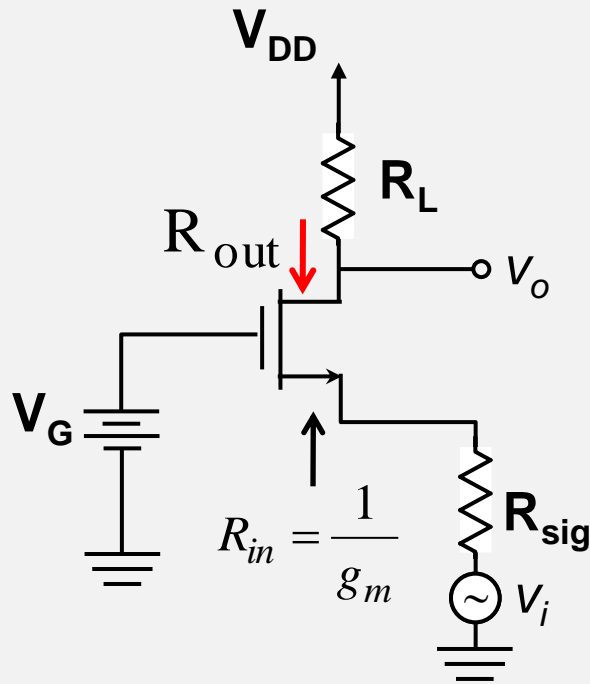
$$= - \left(\frac{-R_{in}}{R_{in} + R_{sig}} \cdot v_i \right) \cdot g_m \cdot \left(R_L \parallel \underbrace{R_{out}}_{\infty} \right)$$

$$\Rightarrow \frac{v_o}{v_i} = \frac{g_m \cdot R_L}{1 + g_m R_{sig}}$$

- With channel-length modulation ($\lambda \neq 0$)

$$\frac{v_o}{v_i} = \frac{g_m \cdot (R_L \parallel R_{out})}{1 + g_m R_{sig}}$$

$$R_{out} = (1 + g_m r_o) \cdot R_{sig} + r_o \approx g_m r_o R_{sig} \quad (\text{if } R_{sig} \text{ is large})$$



在CG中 R_{out} 被提升了，
可利用製作cascode電路

same as the common-source amplifier
with source degeneration (p. 7)

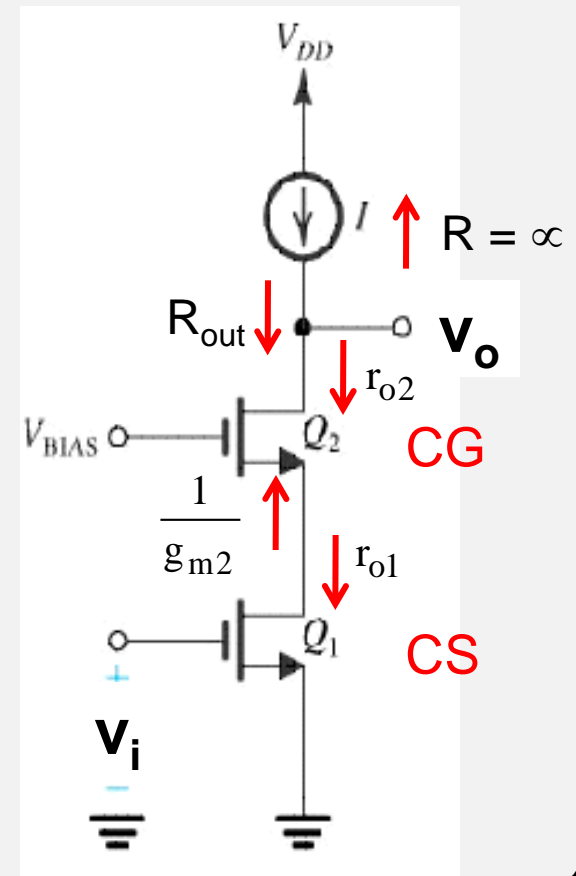
Cascode Amplifier (CS + CG)

- The cascode transistor Q2 provide a low input resistance at the drain of Q1 and a high resistance at the output

考慮上頁的圖:當 $R_L = \infty$, $R_{sig} = r_{o1}$:

$$R_{out} = g_{m2} \cdot r_{o2} \cdot r_{o1}$$

$$\frac{V_o}{V_i} = -g_{m1} \cdot R_{out}$$



Mini Project: 3-Stage Amplifier

注意: $V_{ds} > V_{gs} - V_t$ ，以確保在saturation region工作

$$g_m = \frac{2I_D}{V_{gs} - V_t}$$

